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Icebreaker Windpower Inc.

Application-Part 12 of 13

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• Exhibit BB. Section 106 Geophysical Survey Review for Icebreaker Wind

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Section 106 Geophysical Survey Review for Icebreaker Wind

Prepared for:

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1.0 EXECUTIVE SUMMARY

A geophysical survey of a portion of the Lake Erie lakebed was conducted for the Icebreaker Wind project by Canadian Seabed Research Ltd. (CSR) from mid- August to early September 2016 on behalf of Icebreaker Windpower Inc. Icebreaker Wind is a six turbine 20.7 megawatt offshore wind demonstration project 8 to 10 miles off the shore of Cleveland, Ohio. The data from this survey was evaluated according to Section 106 of the National Historic Preservation Act of 1966 (NHPA) requirements. Three (3) areas of potential effects (APE) were assessed:

- 1. Turbine area 4.7 km (2.9 miles) x 0.3 km (0.2 miles). Beginning about 12.9 km (8 miles) from the mouth of the Cuyahoga River, Cleveland, Ohio, Cuyahoga County, at a depth of 17-18 m (56 59 feet). Within this area six (6) wind turbines will be constructed and interconnected with trenched and buried cables at a depth of about 1.5 m (5 feet).
- 2. Export cable area 13.2 km (8.2 miles) x 0.36 km (0.2 miles). Beginning 1.7 km (1.1 miles) west of the end of the east breakwater offshore of Cleveland, Ohio, Cuyahoga County, and running 13.2 km (8.2 miles) to the Turbine area at a water depth of 10-17 m (33 56 feet). Within this area the export cable from the wind turbines to east breakwater will be trenched and buried at a depth of about 1.5 m (5 feet).
- 3. Inner harbor area 0.85 km (0.53 miles) x 0.36 km (0.22 miles). Beginning 1.7 km (1.1 miles) west of the end of the east breakwater offshore of Cleveland, Ohio, Cuyahoga County, and running 0.85 km (0.53 miles) to shore at the CPP power plant at a water depth of 4-10 m (13 33 feet). Note: The export cable route will be horizontally drilled beginning 1.7 km (1.1 miles) west of the end of the east breakwater on the north side, south to the CPP power plant at a minimum depth of 4 m (12 feet) below the foundation of the breakwater.

The geophysical survey was designed to be in compliance with the guidelines developed by the Bureau of Ocean Energy Management (BOEM) set forth in "Guidelines for Providing Archaeological and Historic Property Information Pursuant to 30 CFR Part 585," compliance with which are directed by the Ohio State Historic Preservation Office (SHPO).

Results from the geophysical survey confirmed that there were no artifacts or properties of historical significance identified at the Icebreaker Wind's APE that would impact the construction of the Project. Nor was there any evidence from the literature search that any artifacts or properties exist at the proposed sites.

VanZandt Engineering recommends that no further archaeological investigation is warranted for the Icebreaker Wind project areas at this time and that clearance for construction be granted.

This report will be submitted to the Ohio SHPO by the U.S. Department of Energy for Section 106 review.

2.0 INTRODUCTION

David M. VanZandt of VanZandt Engineering carried out the Section 106 assessment of the geophysical survey data collected by Canadian Seabed Research from mid- August to early September 2016 for Icebreaker Wind. The following technical report presents the results of this archaeological assessment undertaken to comply with the Section 106 guidelines and the guidelines established by the Ohio State Historic Preservation Office (SHPO) and the U.S. Department of Energy (DOE).

David M. VanZandt, MMA, RPA was responsible for background research, data analysis and interpretation, and report preparation. Mr. VanZandt is qualified as a professional archaeologist by the Register of Professional Archaeologists (RPA), is on the Ohio SHPO historic archaeologists' consultants list, and a member of the Ohio Archaeology Council.

This report details the Section 106 archaeological assessment of the data acquired during the geophysical underwater remote sensing survey conducted by Canadian Seabed Research Ltd. (CSR) for the Icebreaker Wind demonstration project proposed by Icebreaker Windpower Inc. Icebreaker Wind will be the first freshwater offshore wind project in the Great Lakes and in all of North America. The project has three (3) areas of potential effects. The first APE is the Turbine area. The area is 4.7 km (2.9 miles) long by 0.3 km (0.6 miles) wide, bbeginning about 14 km (8.7 miles) offshore of Cleveland, Ohio, Cuyahoga County, at a depth of 17-18 m (56 - 59 feet). Within this area six 3.45 MW wind turbine generators (WTGs) will be located and interconnected with trenched and buried interconnect cables. The interconnect cables will be buried in an excavated trench 1.5 m (5 feet) wide by 1.5 m (5 feet) deep. Each of the WTGs will be supported by a mono-pole substructure atop a suction bucket foundation (mono-bucket). The Mono Bucket (MB), Figure 1, combines the benefits of a gravity base, a monopile, and a suction bucket. It is a Suction Installed Caisson (SICA) or "all-in-one" steel foundation system to support offshore wind turbines. The interface with the lakebed is accomplished by means of a steel skirt that penetrates the seabed. This steel skirt (or bucket) is welded to an upper steel tube and transition piece that resembles the elements above the mudline of a standard offshore wind monopile. The MB skirt for the Icebreaker Wind project will be approximately 17.5 m (57 feet) in diameter and a maximum of 10 m (33 feet) deep.

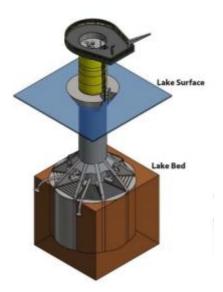


Figure 1 Mono Bucket (MB) Design

The Mono Bucket is installed (Figure 2) by means of both gravity and suction. When the steel bucket is placed on the lakebed, it initially self-penetrates by gravity about 1–2 m (3-6 feet). Suction is then applied and water is pumped from the bucket causing the foundation to penetrate into the lakebed. Once the bucket has achieved the specified penetration, the pump is stopped.

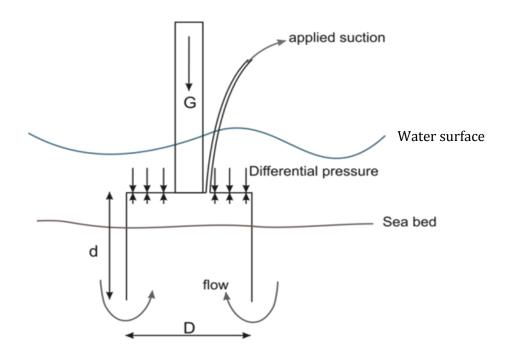


Figure 2 Mono Bucket (MB) Installation

The second APE is the Export cable area. The energy generated from the WTGs will be transmitted through an export cable from the offshore project area to shore. This area is 13.2 km (8.2 miles) x 0.36 km (0.2 miles). Beginning 1.7 km (1.1 miles) west of the end of the east breakwater offshore of Cleveland, Ohio, Cuyahoga County, and running 13.2 km (8.2 miles) to the Turbine area at a water depth of 10-17 m (33 - 56 feet). The export cables will be buried in an excavated trench 1.5 m (5 feet) wide by 1.5 m (5 feet) deep.

The third APE is the Inner harbor area. The export cable will be run in horizontal bore holes generated from Horizontal Directional Drilling (HDD) to allow the cables to pass beneath the Cleveland harbor breakwater and the commercial navigation channel east of Burke Lakefront Airport. The cable will come ashore at the Cleveland Public Power (CPP) Lake Road substation. This area is 0.85 km (0.53 miles) x 0.36 km (0.22 miles). Beginning 1.7 km (1.1 miles) west of

the end of the east breakwater offshore of Cleveland, Ohio, Cuyahoga County, and running 0.85 km (0.53 miles) to shore at the CPP substation at a water depth of 4-10 m (13 - 33 feet). The HDD borehole depth will be a minimum of 4 m (12 feet) below the foundation of the breakwater.

The scope of work includes installing six WTGs assemblies, WTGs interconnect cabling, and export cabling to shore. This work would take 6 months to complete.

3.0 BACKGROUND RESEARCH

3.1 Environmental Context

3.1.1 Bathymetry

The Icebreaker Wind site lies in Lake Erie, the southernmost of the five Great Lakes in North America. The Great Lakes are shown in Figure 3, along with their profiles and surface elevations as the flow of fresh water is traced from Lake Superior to the lower lakes and eventually out into the Atlantic Ocean through the St. Lawrence River (Michigan Sea Grant, 2014).

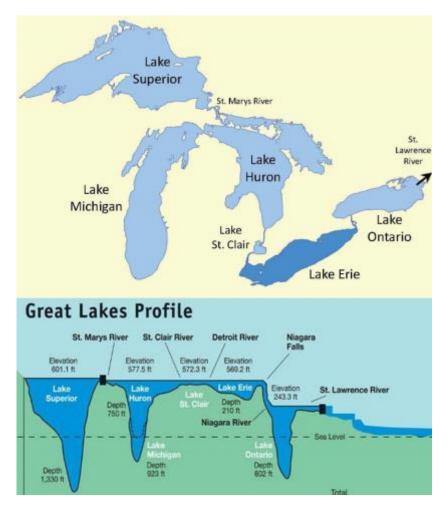


Figure 3 North American Great Lakes (Michigan Sea Grant)

Lake Erie is the shallowest of the Great Lakes with an average depth of 19 m (62 feet) and a maximum depth of 64 m (210 feet) (NOAA, 2014a). It is also the smallest of the Great Lakes by volume (116 cubic miles, or 483 cubic km), although it is only the fourth smallest by surface area (9,910 square miles, or 25,655 square km) (NOAA, 2014a). The water retention or replacement time is 2.7 years, which is short compared to the 6 to 173 years of the other Great Lakes (NOAA, 2014a). An overall bathymetric view of Lake Erie is shown in Figure 4 (NOAA, 2014c).

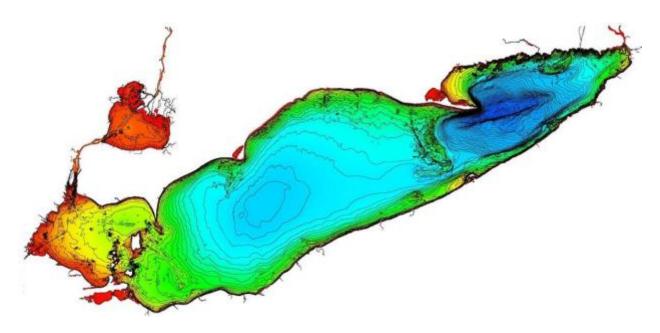


Figure 4 Bathymetric Map of Lake Erie (NOAA)

Lake Erie consists of three distinct regions: the western, central, and eastern basins. Each region has significantly different bathymetric characteristics. The western basin is the shallowest with an average depth of 7 m (21 feet) and features rocky outcrops, shoals, and islands (Waterkeeper, 2014). The central basin has a large flat bottom with an average depth of 20 m (65 feet) and a maximum depth of 24 m (80 feet) in a broad depression in the middle of the Lake (Waterkeeper, 2014)(NOAA, 2014d). In contrast, the eastern basin contains a sharp, deep gouge with several escarpments, an average depth of 24 m (80 feet), and the deepest depths of the Lake off the tip of a long sandy peninsula (Waterkeeper, 2014).

The survey areas (Figure 5) lie between 0 and 20 km (0 and 12.4 miles) offshore of Cleveland, Ohio in the central basin. Corresponding water depths are 5 to 19 m (15-60 feet) relative to the Lake Erie Chart Datum of +173.5 m (NOAA Chart 14829).

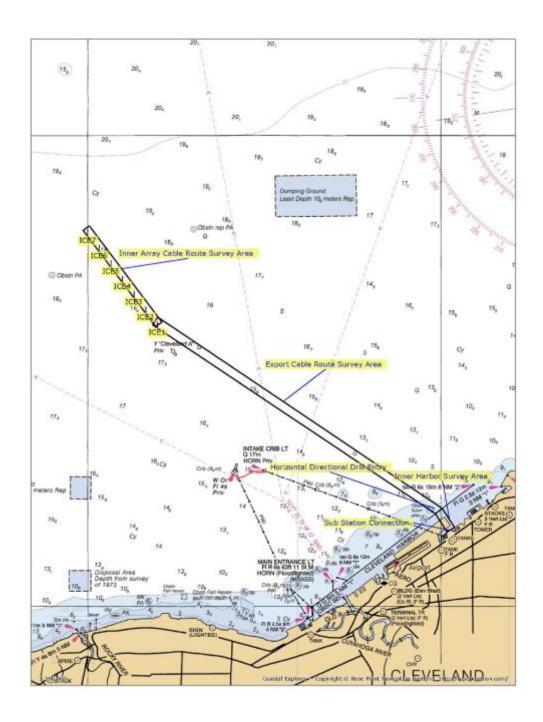


Figure 5 Icebreaker Demonstration Wind Project Site and Bathymetry (VanZandt, NOAA Chart 14829)

3.1.2 Geology

The Great Lakes were formed predominantly by glacial processes. After repeated carving by glaciers during the Pleistocene epoch, only Paleozoic sedimentary rocks remain under

northern Ohio (Dames, 1974). The Paleozoic bedrock exposed under Cleveland is from the Upper Devonian period and roughly dates to between 360 and 380 million years ago (Dames, 1974). This rock is mostly shale and is exposed in cliffs along Lake Erie's shoreline both to the east and west of the City (Carter, 1982). The basin containing Lake Erie itself was carved into this bedrock by repeated Pleistocene glaciations (Dames, 1974). During the last period of Wisconsinan glaciations, the ice moved from the northeast to the southwest to create the lake basin known today (NOAA, 2014d). During the Wisconsinan ice sheet's retreat starting 14,000 years ago and ending 12,600 years ago, glacial till deposits were left behind (Carter, 1982). These deposits are generally unstratified hard clay and gravel called basal till (Carter, 1982). Additional deposits are stratified and clay-rich, and these are called flow till (Carter, 1982). They were created in a deep prehistoric lake that existed until the ice sheet fully retreated (Carter, 1982).

After the start of the Holocene 12,600 years ago, fine-grained lake sediments were deposited above the Pleistocene till layer (Carter, 1982). These post-glacial sedimentary deposits consist of either soft silt or sand in various mixtures. A cross section of Lake Erie water, silt, till, and bedrock is shown in Figure 6 running west to east, through the midpoint of the turbine area, showing the typical subbottom conditions that exist in that area. It should be noted both the bedrock and till layer thicknesses are fairly constant within the boundaries of the 300 meter (1000 foot) width of the survey area.

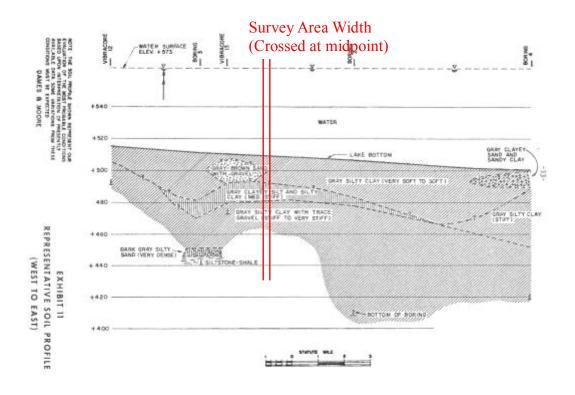
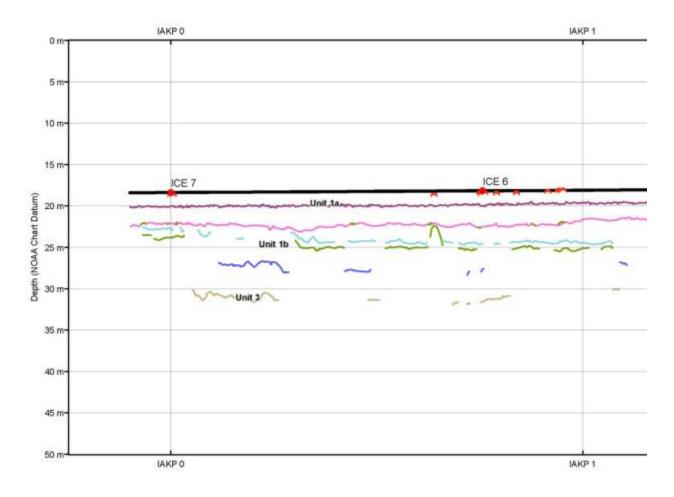


Figure 6 West to East Geologic Cross Section, Lake Erie off Cleveland,
Ohio (Dames & Moore)

The geology along the 4.7 km (2.9 miles) length of the turbine area varied slightly from southeast to northwest. Isopach data for soft clay sediment from the Dames & Moore survey vary from 3 m (10 feet) at the southeastern end to 7.6 m (25 feet) at the northwestern end of the survey area (Dames, 1974). This is comparable with CSR's higher resolution multi-beam subbottom geology survey results of 3 to 7 m (10 to 23 feet) clay sediment layer (Unit 1) from southeastern to the northwestern end (Figure 7) (CSR, 2016, Enclosure 1).



PROPOSED ROUTE PROFILE AND SUB-BOTTOM GEOLOGY



Unit 1 = Post/Pro Glacial Sediments have been subdivided into Units 1a and 1b. Unit 1a consists of soft unconsolidated post glacial sit/clay. Reflector R2 defines the base while R1 represents the boundary between soft sit/clay overlying denser sit/clay. Unit 1b consists of a moderately stiff clay with interbedded sand and silt. The internal reflector R3 represents an organic rich layer. Unit 1 overfles reflectors R4 or R5.

Unit 2 – Glacial Sand/Gravel associated with the Cleveland Ridge. This Unit is bounded by R4 and R5. Point source reflectors interpreted as boulders occur throughout this unit exposed at the lakebed.

Unit 3 – Glacial Clay with Sand and Gravel deposited in a glacio-lacustrine environment. This Unit is bounded by reflectors R5 and B1. Internal reflector R7 is the deepest reflector observed within the chip profiler data.

Unit 4 - Undifferentiated Glacial Sediments. This unit is bounded by B1 and acoustic basement.

Figure 7 Typical Sub-bottom Geology Turbine Area (CSR)

The geology along the 13.2 km (8.2 miles) length of the export cable area varied slightly from southeast to northwest. The soft clay sediments (Unit 1) vary from 0 m at the southeastern end to 3 m (9 feet) at the northwestern end of the export cable area (CSR, 2016, Enclosure 2-4).

The glacial sand/gravel sediments (Unit 2) average about 5 m (15 feet) for the export cable area (CSR, 2016, Enclosure 2-4). These sediment layers are much deeper than the trench depth of the export cable of 1.5 m (5 feet).

3.1.3 Flora and Fauna

Lake Erie is the most biologically productive of all of the Great Lakes and contains a large, active freshwater fishery (Waterkeeper, 2014). The lake's productivity is due mostly to the large abundance of phytoplankton, small plants in the water column which form the basis of the food chain (NOAA, 2014b). The warm lake water temperatures due to the relatively shallow depths and an abundance of nutrients from rivers help the phytoplankton thrive. Green alga, a single celled plant, is the most important and the basis of the summer food web (NOAA, 2014b). Diatoms, flagellates, and blue-green algae (cyanobacteria) are also present, especially in the early spring or late summer months (NOAA, 2014b). An overabundance of both phosphoric nutrients combined with rain events, and summer sunlight can lead to algae blooms. These have posed significant environmental problems during recent years.

The phytoplankton serves as food for a variety of creatures in the Lake, including zooplankton and macroinvertebrates (NOAA, 2014b). Zooplankton, small animals in the water column, feed on both the phytoplankton and each other (NOAA, 2014b). Macroinvertebrates (larval insects, worms, amphipods, or mollusks) feed on the phytoplankton or detritus on the bottom (NOAA, 2014b). Foraging fish (perch, shad, drum, catfish, carp, and gobies) eat both the zooplankton and macroinvertebrates (NOAA, 2014b). These fish are then eaten by the piscivores, or the top predatory fish, such as walleye, bass, and trout (NOAA, 2014b).

Figure 8 illustrates the food web of Lake Erie (NOAA, 2014b). At the bottom of the web are the phytoplankton colored in green. The next level is comprised of the zooplankton and macroinvertebrates colored in light blue and orange, respectively. The third level is made up of the foraging fish shown in dark blue, and the top level includes the piscivores colored in purple.

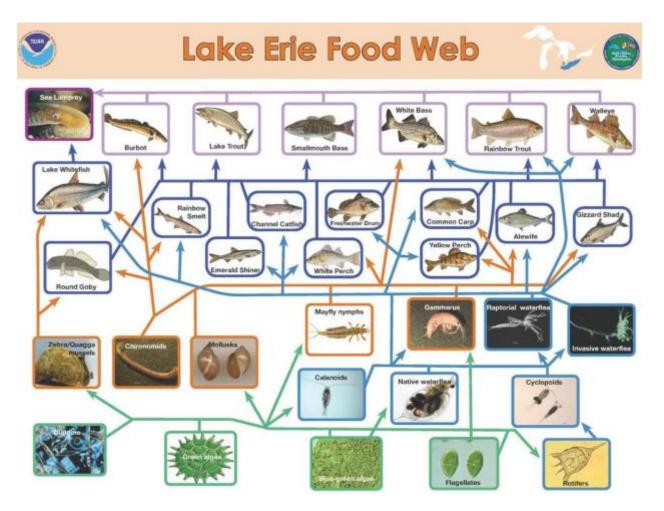


Figure 8 Lake Erie Food Web (NOAA Great Lakes Environmental Research Laboratory)

3.2 Prehistoric Context

Any prehistoric artifacts or structures predating the Holocene Epoch were either destroyed or scattered during glaciations that occurred during that time. The last of the glacial ice sheets, the Wisconsinan's, began retreating during the Pleistocene Epoch ~14,000 years before present (YBP) and ended ~12,600 YBP with glacial till deposits being left behind (Carter, 1982). These deposits generally consist of unstratified hard clay and gravel that are called basal till (Carter, 1982). Additional deposits are stratified and clay-rich, and these are called flow till (Carter, 1982). These deposits were deposited over the Lake Erie basin's shale layer. The thicknesses of the glacial till in the survey area have a range of 55 to 93 feet (Dames, 1974) and 53 to 85 feet (Alpine, 2010).

After the start of the Holocene ~12,600 YBP, fine-grained lake sediments were deposited above the Pleistocene till layer (Carter, 1982). These post-glacial sedimentary deposits consist of either soft silt or sand in various mixtures. The thickness of these soft silt and clay deposits in the survey area vary from 10 to 25 feet (Dames, 1974) and 10 to 16 feet (Alpine, 2010).

During the period from ~12,000 YBP to ~5,400 YBP the lake level was below the turbine APE, which has an elevation at the glacial till layer of +492 feet, thus exposing the land for possible human habitation or use. The lake level during that period varied from +394 feet during the post glaciations Early Lake Erie stage to +476 feet during the Middle Lake Erie stage, ~7,500 YBP (Herdendorf, 2013). At the start of the Middle Lake Erie stage, ~5,400 YBP, the lake level had risen to +525 feet, which inundated the turbine APE, placing any possible prehistoric occupation site underwater (Herdendorf, 2013). After the Middle Lake Erie stage the lake level continued to rise to its present day level of +569 feet (Herdendorf, 2013).

Paleoindian occupation of Northern Ohio was believed to have occurred between 13,000 to 11,000 YBP (Herdendorf, Klarer, Herdendorf, 2006). The earliest evidence in Ohio of occupation is at the Paleo Crossing site (33ME274) in Medina County, Ohio, which has been dated between 10,000 to 11,500 YBP (Brose, 1994).

It is possible that artifacts from early occupation could exist buried at the proposed site, but to date Lake Erie has not been a focus of archaeological research on Paleoindian culture (Stothers, Abel, 2001).

"Paleoindian sites present a very low archaeological profile across the landscape and are representative of areas where small groups of people would perform specific tasks of short duration. Additionally in northern Ohio, Stothers and Pratt (1980) note that Early and Middle Archaic sites are usually of two types: "those in which a single or a few points are included in a collection of material from other cultural periods, and those in which Early or Middle Archaic materials predominate." The later, mixed sites, would not be represented in the areas examined. The potential for locating Early and Middle Archaic sites beneath Holocene lake sediments with today's remote sensing technologies is a factor of sedimentation depths and relict landscapes. Features such as hidden outcrops that may indicate cultural use areas, have been covered by natural lake sedimentation processes. Therefore, it would be difficult or impossible to locate sites if they existed (Gray & Pape, 2014)."

3.3 Historic Context

Lake Erie has been instrumental in historical shipping and transportation in the Great Lakes. The permanent settlement of the Ohio shores of Lake Erie occurred at a slower pace than that of the Ohio or Mississippi valleys due to the control of the lake by Great Britain (Mansfield, 1899). It wasn't until 1796 that the British relinquished control of their post commanding Lake trade (Mansfield, 1899). Since the opening of the Erie Canal in 1826 from the Hudson River to Buffalo, New York, Lake Erie has served as the crucial nexus for shipping into the upper Great Lakes region and eventually points further west. Immigrants and goods moving westwards would start in New York City; move up the Hudson River by ship, travel along the Erie Canal by boat, and then board yet another ship in Buffalo for transportation down the length of the Lake. At first, Lake Erie was the earliest of the Great Lakes' destination as immigrants from Europe and the Northern States began to settle along its shores. Eventually, however, passengers and goods continued on to the other lakes and, ultimately, Chicago, which then served as the starting point for further western expansion (Mansfield, 1899). It was estimated in 1832 that more than half of the immigrants arrived in the West by water (Mansfield, 1899).

As settlers grew crops, harvested timber, and mined copper and iron ores, these products flowed eastwards back down the lakes and across Lake Erie to be delivered to the east coast. Meanwhile, coal from Pennsylvania, new immigrants, and finished manufactured goods continued to travel westward across Lake Erie from Buffalo. In order to deliver these people and goods, many hundreds of ships operated on the Great Lakes every season in the 19th century (Mansfield, 1899). These ships were frequently made of wood and lacked radio, radar, or modern electronic navigational aids. Furthermore, there was a general lack of accurate weather forecasting, detailed bathymetric information, and other useful aids to safety. As a result, many unfortunate vessels collided with each other, ran aground, sprang leaks, caught fire, or foundered in storms. Lake Erie is the shallowest of all the Great Lakes and is known to have especially severe waves due to its lack of depth and prevailing winds, which blow along the length of the Lake and have caused many ships to succumb to its depths. The end result is a high number of shipwrecks, possibly numbering in the thousands, in Lake Erie (Frew, 2014).

The exact number and location of these shipwrecks is unknown because of the lack of accurate records for these events. There is no central governmental repository that records sinkings. In many cases the only record of a shipwreck may be a story in a local town or city newspaper. Official records are split among two national governments (United States and Canada) and multiple governmental agencies and archives, making an accurate accounting nearly impossible. This is further exacerbated by the fact that many ships were raised and put back into service without as much publicity as surrounded their sinking events, making the total number of shipwrecks left on the bottom even more uncertain. Currently, there are about 250 known shipwrecks in Lake Erie and more are found regularly (ODNR, 2009). Estimates put the total number of shipwrecks in Lake Erie at between 500 and 3,000 (Frew, 2014) (ODNR, 2009).

Historic shipwrecks consist of both wooden and metal ships, sailing vessels, sidewheel steamers, and propeller steamers. The cold fresh water of the Great Lakes tends to serve as an excellent preservative for these wrecks. There are no wood-eating organisms, such as the Teredo worm found in warm ocean environments. Cold water greatly inhibits bacterial decay, allowing wooden timbers and grain cargos to survive. The fresh water is also much less corrosive on metal artifacts, unlike the salty oceans, and the inland seas do not have storms as destructive as ocean-borne hurricanes and typhoons. Thus, many of the shipwrecks in the Great Lakes serve are well preserved archaeological sites that provide significant information about 19th century shipbuilding, shipboard life, and the associated maritime landscape associated with these wrecks.

3.4 Literature Review

VanZandt Engineering consulted the Ohio Historic Preservation Office (OHPO) online mapping system in an effort to locate any inventoried cultural resources identified within the survey area. The archival study included a review of the Ohio Archaeological Inventory (OAI), Ohio Historic Inventory (OHI), the National Register of Historic Places (NRHP), Ohio Sea Grant Shipwreck map, the Cleveland Underwater Explorers shipwreck data base, and the Cleveland Underwater Explorers historical Lake Erie nautical chart collection. Four previously-inventoried cultural resources (shipwrecks) have been identified within 3.5 nm of the survey area. These shipwrecks were the *Admiral* and *Dundee* (3.0 and 3.3 nm, respectively, from the northwest survey corner point), and the CSU wreck and East Breakwall Barge (0.5 and 1.6 nm,

respectively, from the export cable area). None of these wrecks were detected within the survey area.

Results of the literature review are described below:

Ohio Archaeology Inventory:

No properties listed on the Ohio Archaeology Inventory are present within the survey area.

Ohio Historic Inventory:

No properties listed on the Ohio Historic Inventory are present within the survey area.

National Register of Historic Places:

No individual properties or districts listed on or determined eligible for listing on the NRHP are present within the survey area.

Ohio Sea Grant Shipwreck Map:

No shipwrecks on the Ohio Sea Grant Shipwreck map are present within the survey area. Four shipwrecks are located within 3.5 nm of the survey area. These shipwrecks were the *Admiral* and *Dundee* (3.0 and 3.3 nm, respectively, from the northwest survey corner point), and the CSU wreck and east breakwall barge (0.5 and 1.6 nm, respectively, from the export cable area). The shipwreck map shows the possibility of the *Dreadnaugt* (probably *Dreadnaught*) and the *Mackinaw* being close to the survey area, but these locations are unconfirmed and based off of shipwreck maps that were for sale to the public. Most of the locations derived from these maps are not verified, and therefore the ODNR did not base their offshore wind farm siting analysis on them. See, Wind Turbine Placement Favorability Analysis Map Methodology (ODNR, 2009).

Further historical research on both shipwrecks show that the *Dreadnaugt* came ashore and was abandoned and the *Mackinaw* was farther from the project APEs than the shipwreck map indicated. Thus, neither would be close to project APEs. The Cleveland

Underwater Explorers (CLUE) has recently discovered what they believe are the remains of the *Mackinaw*, and it is its located 4.4 nm east of the project site.

Cleveland Underwater Explorers Shipwreck Data Base:

No shipwrecks in the Cleveland Underwater Explorers shipwreck data base are present within the survey area.

Cleveland Underwater Explorers Historical Lake Erie Nautical Chart Collection:

No shipwrecks were found charted on any chart in the Cleveland Underwater Explorers historical Lake Erie nautical chart collection within the survey area or within 3.5 nm of the survey area.

4.0 METHODS

4.1 Survey Design

The main objectives of the survey were to identify and map surficial geology, lakebed features and sub-bottom conditions within the WTG area and the proposed submarine cable routes.

The objectives of the geophysical survey were accomplished by the collection, interpretation and subsequent reporting of geophysical data. The following types of data were collected during the marine geophysical survey (CSR, 2016):

- Differential GPS navigation was constantly recorded to provide real-time georeferencing for all data sets acquired during the survey.
- Sidescan sonar data were acquired to identify potential hazards exposed on the surface of the lakebed (shipwrecks, pipelines, boulders, debris, ice gouging) and to categorize surficial sediment types.
- High-resolution chirp profiler data were acquired throughout the geophysical program to identify the sub-bottom geology to a depth of at least 5 m (15 feet).
- Lakebed bathymetry data was continuously logged throughout the geophysical program using a multibeam echosounder in order to determine water depths (lakebed elevations) along the route.
- Marine magnetometer data were collected to identify surface and buried ferrous targets.
- Grab samples were collected to ground truth the surficial geology interpretation.
- High resolution 50 kHz profiler data was collected over the proposed turbine locations to aid the interpretation of the near surface unconsolidated sediments.
- High-resolution single channel seismic (mid penetration "boomer") data were acquired within the Harbor and near shore areas to aid the interpretation over the HDD location.
- Sidescan sonar and magnetometer data were not collected in the harbor since the
 cable will be installed at depth within a HDD casing and therefore there was no
 requirement for archaeological clearance.

4.2 Overall Survey Layout

4.2.1 Turbine Area

Survey coverage over the Turbine Area included a 240 m (720 feet) corridor centered on the proposed route extending from WTGs ICE1 to ICE7. Overall, 22 lines were surveyed totaling 47 line km. Tie line spacing was 375 m (1,125 feet) along the Turbine Area. Figure 9 illustrates the geophysical survey track lines in the Turbine Area (CSR, 2016).

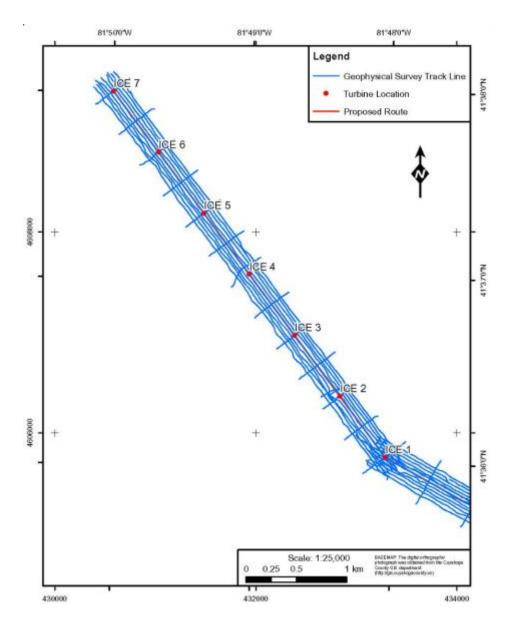


Figure 9 Geophysical survey track lines over the Turbine Area. (CSR)

4.2.2 Export Cable Area

Survey Coverage over the Export Cable Area included a 300 m (990 feet) corridor centered on the proposed route. The Export Cable Area extends from the proposed HDD exit location to WTG ICE1. The survey area was expanded north of the breakwater to TP1 and TP2 to ensure that enough data was acquired to accommodate alternative HDD exit locations. Additional lines were surveyed parallel to the breakwater to gain more information in the HDD exit area, and to map the toe of the breakwater slope. Overall, 73 geophysical survey lines were run totaling 206 line km. Figure 10 illustrates the geophysical survey track lines along the Export Cable Area (CSR, 2016).

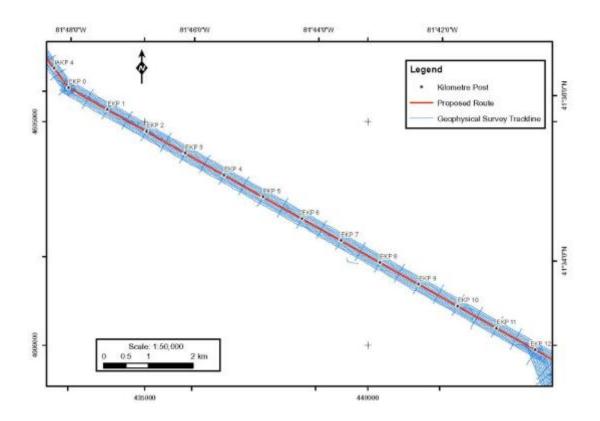


Figure 10 Geophysical survey track lines along the Export Cable Area. (CSR)

4.2.3 Inner Harbor Area

The geophysical survey lines were designed for the collection of multibeam sonar and sub-bottom profiler data along potential HDD routes between the Cleveland breakwater and the landfall. A total of 26 lines were surveyed, totaling 18 line km. Figure 11 illustrates the geophysical survey track lines within the harbor area (CSR, 2016).

Sidescan sonar and magnetometer data were not collected in the harbor since the cable will be installed at depth within a HDD casing, and therefore there was no requirement for archaeological clearance (CSR, 2016).

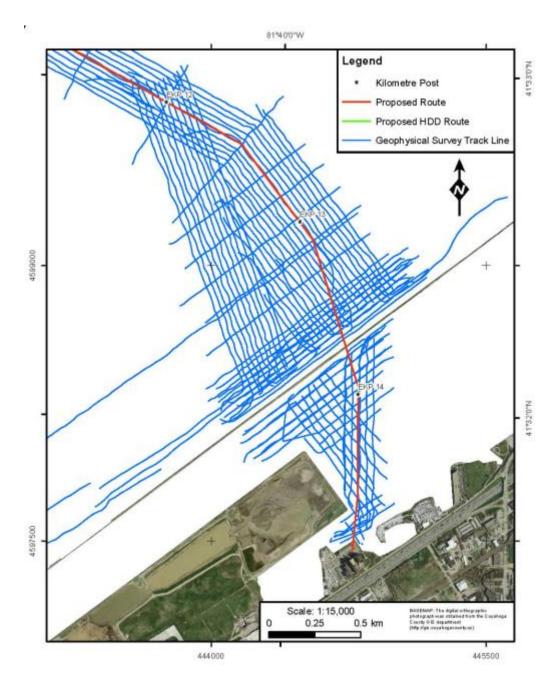


Figure 11 Geophysical survey track lines within the Harbor and over the near shore HDD exit Location. (CSR)

4.2.4 Locational Data:

Note: Locational data in decimal degrees, WGS84 geodetic and UTM, NAD27, Zone 17, M

Table 1 Wind Turbine Generator Locations:

ICE1 N41.60072 W81.80055 433273.438E 4605537.801N

ICE2 N41.60616 W81.80602

432823.244E 4606146.037N

ICE3 N41.61159 W81.81150

432372.284E 4606753.200N

ICE4 N41.61702 W81.81697

431922.235E 4607360.384N

ICE5 N41.62246 W81.82245

431471.440E 4607968.716N

ICE6 N41.62789 W81.82793

431020.712E 4608575.966N

ICE7 N41.63333 W81.83340 (Backup site)

430570.906E 4609184.348N

4.3 Field Methods (CSR, 2016)

The following section describes the methodologies and equipment used to perform the data collection task required for the survey. Survey design and control was based on the guidelines developed by the Bureau of Ocean Energy Management (BOEM) set forth in NTL No. 2005-G07.

4.3.1 Vessel

The Survey operations were conducted from Underwater Marine Contractors Inc. vessel *Salvage Chief* (Figure 12). The *Salvage Chief* is steel constructed, with an overall length of 49ft. The *Salvage Chief* had ample deck space with a knuckle boom and an extendable hydraulic A-frame, ideal for mounting winches and the deployment/recovery of geophysical equipment. CSR installed over-the-side mounts for dual frequency single beam and multibeam transducers on the starboard side of the Salvage Chief. Electronic equipment and data collection workstations were set up in the vessel's wheelhouse (CSR, 2016).

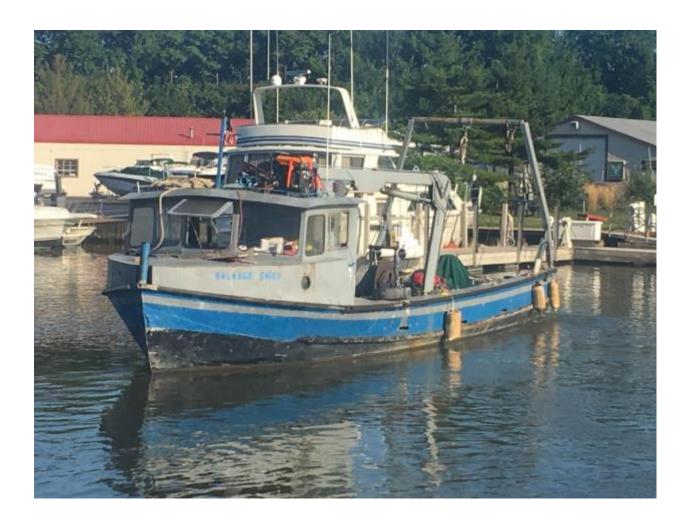


Figure 12 Salvage Chief (CSR)

4.3.2 Survey Reference

Horizontal positioning was calculated using Differential Global Positioning System (DGPS). The primary Coast Guard differential corrections were acquired from the Detroit, MI reference station. The geodetic parameters for the survey were as follows (CSR, 2016):

- Vertical Datum: Lake Erie Chart Datum (173.5 m or 569.2 ft. above IGLD 1985)
- Horizontal Datum: NAD83
- Projection: Universal Transverse Mercator, Zone 17
- Central Meridian 81°W

• False Easting: 500000.00

• False Northing: 0.000000

• Scale Factor: 0.999600

• Latitude of Origin: 0.0

• Linear Unit: Meter

4.3.3 Navigation Control

A real-time DGPS system was utilized during the geophysical survey. CSR's integrated navigation system consisted of a Hemisphere VS-330 DGPS system and the Hypack survey navigation package. The integrated navigation system included real time digital data logging of positional data, a left/right steering monitor for the helmsman, and an interface to the geophysical equipment so that all data was correctly geo-referenced (CSR, 2016).

• Hemisphere VS-330 GNSS Receiver & Heading System

The Hemisphere VS-330 is a dual antenna DGPS system with a horizontal accuracy of 0.3 m (1 foot) under ideal conditions. The secondary antenna (forward) is used to calculate heading to an accuracy of 0.09° RMS. The system was configured to receive Coast Guard differential corrections from Detroit, MI, which operates on a transmission frequency 319 kHz. Positions for the multibeam bathymetry were calculated based on the offset from the primary Hemisphere DGPS antenna, to the multibeam transducer (CSR, 2016).

• Hemisphere R110 DGPS

The Hemisphere R100 DGPS system was used in tandem with the Hemisphere VS-330 during the geophysical survey operations. The system was configured to receive Coast Guard differential corrections from Detroit, MI. The Hemisphere R100 is a single antenna GPS system with a horizontal accuracy of 0.6 m (2 feet) under ideal conditions (CSR, 2016).

Positions for the single beam bathymetry were calculated based on the offset from the Hemisphere R110 DGPS antenna to the transducer. Hemisphere R110 DGPS positioning combined with vessel heading and offset measurements were also used to georeference the

sidescan sonar, chirp, and magnetometer data collected during the survey. Cable out measurements were recorded by the operator during the survey for each line with layback corrections applied during processing and interpretation (CSR, 2016).

• Hypack/Hysweep Survey Acquisition Software

Hypack is a complete hydrographic survey navigation software package that includes: survey preparation, data collection, data editing, cross-section display, geodesy and exporting capabilities. In operational survey mode, the system supports a helmsman display with survey line indicator, to assure survey lines are followed as accurately as possible. In addition to planned survey grid lines, the survey screen also displays bathymetric contours, coastline, navigational hazards, and target/sample locations. During survey operations all navigation information was logged in Hypack to ensure simultaneous geo-referencing of all datasets (CSR, 2016).

4.3.4 Survey Equipment

• SURVEY NAVIGATION

- o Hemisphere VS-330 GNSS Receiver & Heading System
- Hemisphere R110 DGPS Receiver
- HYPACK Survey Navigation Software

MULTIBEAM ECHOSOUNDER

- o Teledyne-Odom ES3 Multibeam Echosounder (240 kHz)
- Teledyne-TSS DMS-05 Motion Sensor
- o Teledyne-Odom DigiBar-Pro Velocimeter
- Applied Microsystems SVPlus
- HYSWEEP Multibeam Acquisition System

• SINGLE BEAM ECHOSOUNDER

Odom CV3 Dual Frequency Echosounder (50/200 kHz)

SIDESCAN SONAR

- o Klein 3000 (100/500 kHz) Sidescan Sonar System
- SonarPro Sidescan Acquisition Software

• MAGNETOMETER

o Marine Magnetics SeaSPY Marine Magnetometer

• SUB-BOTTOM PROFILER

o Klein 3000 Chirp Profiler (2-8 kHz)

SEISMIC REFLECTION

- o EG&G 240 Low Frequency (400-14,000 Hz) Shallow Seismic System (Boomer)
- Applied Acoustics CSP-300 Power Supply
- o Ministreamer with GeoSpectrum M5 Hydrophones
- SonarWiz SBP Acquisition & Processing Software

• TIDE GAUGE

- HOBOware U20 Titanium Water Level Data Logger
- SAMPLING
- Van Veen Grab Sampler

4.3.5 Side Scan Sonar Survey

A Klein 3000 dual frequency sidescan system was used to complete the seabed imaging component of the Icebreaker Wind cable route assessment. The Klein 3000 consisted of a sonar instrumented towfish, a transceiver and processing unit (TPU) and an acquisition computer running Klein's proprietary Sonar Pro software. Capable of simultaneous dual frequency operation (100/500 kHz) and constructed with advanced electronics and transducers, the Klein 3000 produced superior high resolution imagery of the seafloor. High frequency (500 kHz) ranges of between 75 and 100 m on both the port and starboard channels allowed for wide area swath coverage and target detection over the route.

Frequency: 500 kHz

Range Setting: 75 m and 100 m range

Target Resolution: 10-20 cm in ideal conditions

Lane Size: 27 m

Tow Height: 5 to 6 m above the lake bottom

Rationale: 100% seafloor coverage; target detection & surficial geology mapping

During the 2016 geophysical survey, the sidescan system was integrated with the Klein 3000 chirp profiler and marine magnetometer. When the sidescan system is integrated with the chirp profiler only one frequency can be recorded. For this survey the higher 500 kHz frequency was acquired.

Calculated layback measurements were used to position the sidescan sonar system during interpretation and mapping of the data. Layback is calculated using the offset between the DGPS antenna and tow point, the height of the tow above the water line, the depth of the system below the surface, and the length of cable deployed. Where possible, feature matching between the sidescan, sub-bottom profiler and multibeam data was used to confirm layback calculations.

SonarPro was used to operate the Klein 3000 sidescan sonar and chirp systems. The system provides navigational recording, target management, and real-time display of the sidescan data. SonarPro also provides the options to adjust the towfish sensors during data acquisition, including range and transmit power, which is directly recorded with the raw data. The target management feature enabled the selection of seabed targets in both real-time and during playback following collection. The sidescan and chirp data were recorded to XTF format (CSR, 2016).

4.3.6 Magnetic Survey

A Marine Magnetics SeaSpy Magnetometer was used for the survey. The SeaSpy is a digital marine magnetometer that operates using an advanced Overhauser sensor. Measuring the ambient magnetic field, using a specialized branch of magnetic resonance technology, the SeaSpy has an absolute accuracy of 0.2 Nanotesla (nT). The sensor is capable of measuring a range of 18,000 nT to 120,000 nT in all directions, resulting in no dead zones and reliable data.

During the 2016 geophysical survey, the marine magnetometer was integrated with the Klein 3000 system (CSR, 2016).

4.3.7 Sub-bottom Mapping System

Sub-bottom geophysical data was acquired using two systems, a chirp profiler and a single channel seismic system (CSR, 2016).

The Klein system uses two Chirp transmit transducers with a single linear hydrophone. The Mills Cross configuration achieves higher resolution and deeper bottom penetration than comparable systems. The Klein 3000 chirp sub-bottom profiler (SBP) integrates with the Klein 3000 sidescan system. It mounts directly to the Klein 3000 tow vehicle and uses the existing physical connections and electrical communications. This option takes advantage of the existing Klein 3000 sidescan hardware by using the same tow cable, transceiver processor unit (TPU), workstation and towing systems. The chirp sub-bottom profiler consists of a subsea assembly used to contain the transmit projectors, receive hydrophone and SBP electronics. These components are enclosed in a fiberglass shroud with an integrated support structure to allow for combined transducer/electronics mounting and towing. The Klein 3000 tow vehicle installs into the rear portion of the shroud assembly where it interconnects with the SBP electronics. The amplifier modulates both amplitude and phase of the transmit waveform for pulse lengths up to 40 msec.

Specifications:

Chirp Frequency: 2-8 kHz

Beam Angle: 20° along track; 40° cross track @ 5 kHz

Resolution: 12.5 cm or better

Power: 1 kwatt

Source Level: 204 db @ 1 m

CSR has achieved penetration of up to 100 m (330 feet) with this system in fine grained sediments. During this survey the maximum penetration achieved was 15 to 20 m (49 to 66 feet) within post glacial and glacial fine grained sediments. The chirp signal was impeded in areas where shallow gas and coarse grained glacial sediments occurred.

30

Additional survey data were collected using a single channel seismic (Boomer) system. This system provides low frequency energy in the range of 400-10,000 Hz and includes four main components (boomer plate, power supply, hydrophone, and acquisition computer). The energy source for the system was the Applied Acoustics CSP-300 which has output settings ranging from 50-300 joules. The CSP supplied power to the boomer plate, which was towed in conjunction with a low frequency hydrophone streamer. The boomer plate was responsible for transmitting the sound energy through the water column and lakebed sediments. The hydrophone streamer received the reflected sound energy, transmitting the signal to the topside recording computer.

The raw and processed acoustic signal was recorded on a topside computer running SonarWiz acquisition software. DGPS positioning information was integrated with the data in real-time and recorded by SonarWiz in seismic data SEG-Y format. Acoustic frequency filters applied to the data in real time using SonarWiz were not recorded to the raw data. The frequency filters essentially "cleaned" the data allowing for better visualization and interpretation of the sub-surface sediments. Low- Cut (400 Hz) and High-Cut (4000 Hz) frequency filters were applied to the data in real time using the SPA-3 processing unit. This data was recorded to a second channel within the SGY file. In addition to filter processing, the SPA-3 unit (IKB Technologies Ltd) also controlled the firing rate of the boomer system.

During this survey the energy source was operated at an output level of 100, 200, and 300 joules with a firing rate of 1/4 second (100 joules) and 3/8 second (200 & 300 joules). The record length was synced to the firing rate within SonarWiz.

CSR has achieved penetration of greater than 100 m (330 feet) with this system in fine to coarse grained sediments. During this survey the maximum penetration achieved was 50 to 60 m (165 to 198 feet) within post glacial and glacial sediments over the HDD survey area. The boomer signal was impeded in areas where shallow gas and acoustic basement (interpreted to be bedrock) occurred.

4.3.8 Personnel

Party Chief Colin Toole, CSR

Hydrographic Surveyor Luke Melanson, CSR

Electronics Technician Jon MacDonald, CSR

Vessel Captain Joel Frazer, Underwater Marine

5.0 DATA ANALYSIS

5.1 Sidescan Sonar Data Analysis

A review of 271 line km of sidescan data showed no historic structures (such as shipwrecks) or artifacts were present within the turbine (Figure 13) and export cable (Figure 14) survey areas. (Note: For full size images see appendices)

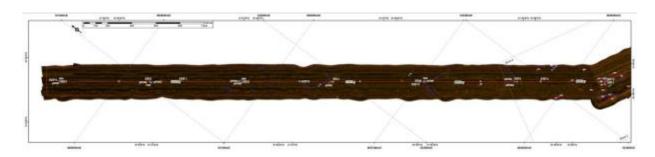


Figure 13 Turbine Survey Area Sidescan Mosaic. (CSR)

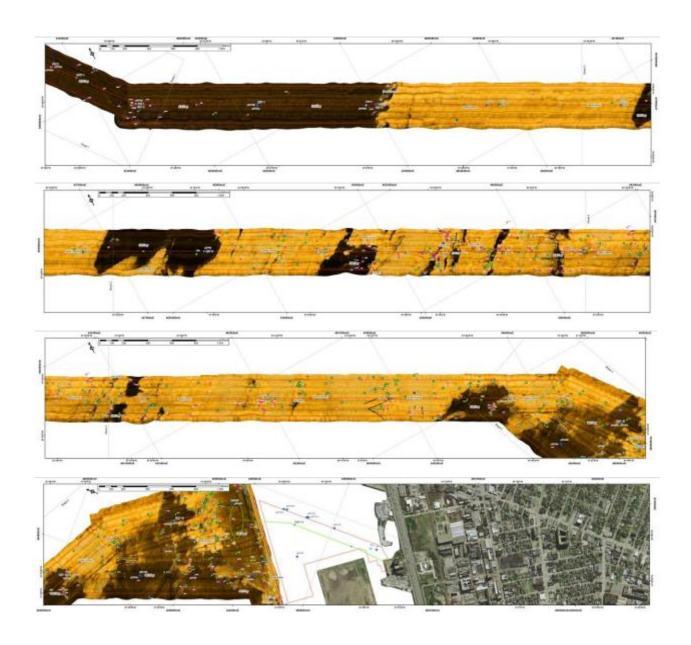


Figure 14 Export Cable Survey Area Sidescan Mosaic (CSR)

The Side Scan Sonar showed a generally uniform and smooth lake bottom. Some evidence of ripples or other sedimentary features were observed along the survey route (Figure 15) and some areas of the bottom revealed enhanced reflectivity denoting a change in geological structure (Figure 16). These locations were assigned a target number, and corresponding imagery and information can be found in Appendix A.

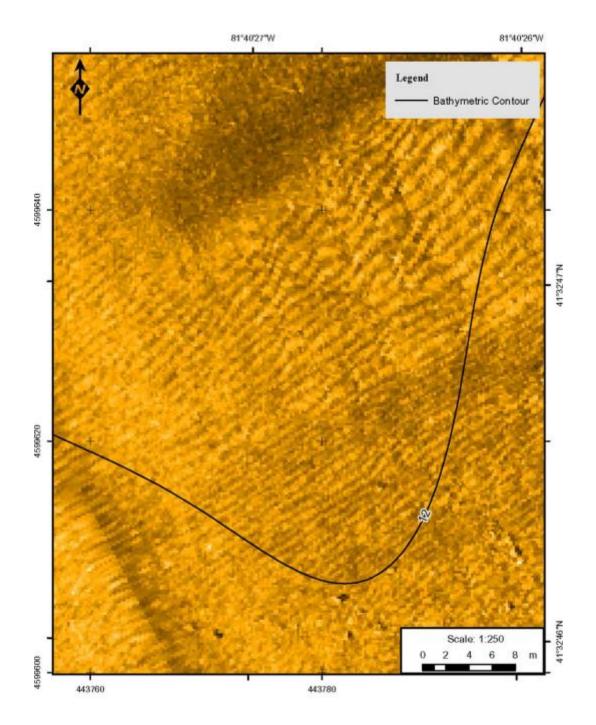


Figure 15 Sediment Rippling along Export Cable Route (CSR)

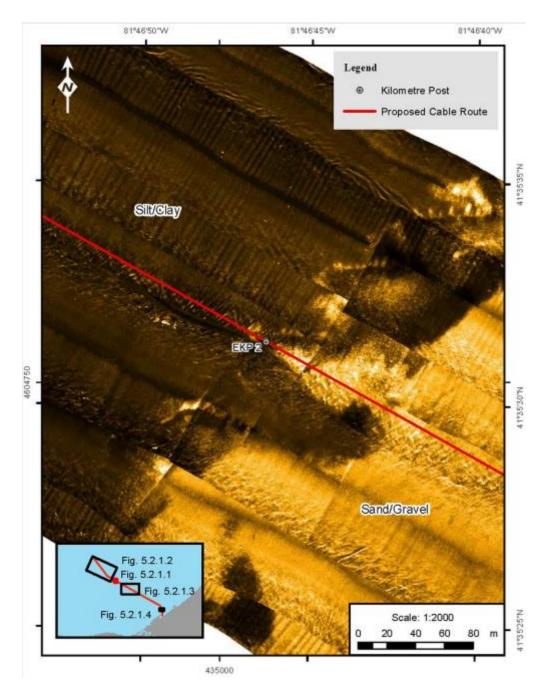


Figure 16 Sidescan Sonar Data Illustrating the Surficial Boundary between the Cleveland Ridge Sand/Gravel and Post Glacial Silt/Clay, EKP 2. (CSR)

The only targets identified were geological or the result of old trash dumpings (rectangular, circular, and linear contacts) and dredge spoil (circular contacts) in the survey areas (Figure 17). A total of 455 identified targets were analyzed and the detailed description of the targets can be found in Table 2 (Locational data in NAD83 Geographic, NAD83, Zone 17, M, and NAD83, Ohio State Plane North, US Survey Feet). See Appendix A for complete target data

with images. There are a number of targets that may indicate the presence of a linear ferrous feature perpendicular to the proposed route. This feature could not be identified from the sidescan or sub-bottom profiler data acquired over this area. An analysis of the magnetic data shows that these targets are most likely buried steel or iron buoy blocks or anchors.

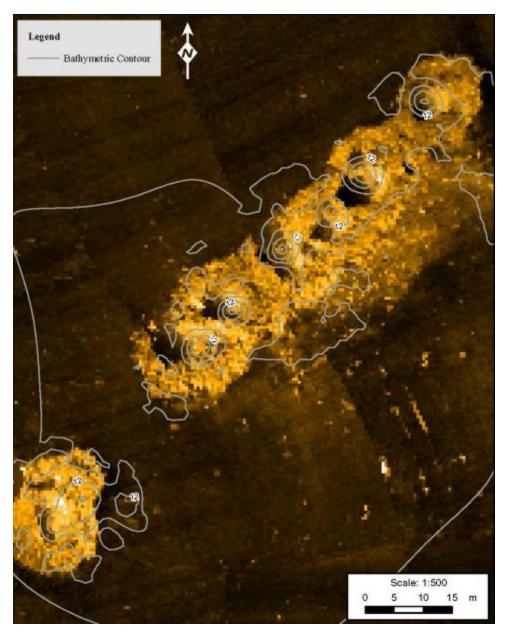


Figure 17 Sidescan Sonar Record of Dredge Spoil. Center of Data Example is Located 150 m E of EKP 12. (CSR)

Table 2 Sidescan Sonar Contacts List

	MADES 0	ieographic	MADES U	TIM Zone 17	MADES Ohio S	Side Sate Plane North	can Senar Con	Distance from			900.00		la managara and
ID	Latitude	Longitude	East(m)	North (m)	East (US survey feet)	North (US survey feet)	Bathymetry (m)	Proposed Route (m)	(m)	Width (m)	Height (m)	Description	Associated May Anomaly ID
a	41.6176299		431841.5	4607646.7	2154951.3	711527.0	17.8	35.5	2.6	0.5	0.2	Linear Contact	-
a		-81.9170325		4607594.3 4607095.8	2155248.0	711327.6	17.7	51.6	2.5	0.2	-	Linear Contact Point Source (Probable Buoy	
G	41.6127124	-81.0118403	432358.2	4007095.8	2156878.1		17.8	21.0	2.5	1.0	\$100.0	Mooning) Circular Contact (Probable	1.7
C#	41.6114662		3302.13117.	4606957.2	2156769.2	709295.5	17.5	10.6	7.4	7.0	***	Beoy Mooring)	
CS CS		-81.8060026 -81.8026018	432838.4 433120.1	4606358.7 4606167.0	2159295.7	707357.3 706744.1	17.8	1.6	3.9	3.5	0.6	Greuler Contact Point Source	M84
C7		-81.9035480		4606163.1	2159245.5	706791.8	17.2	111.8	1.8	0.8	0.6	Point Source	1100
CE	41,6006765	-81.8006100	433262.2	4605750.0	2159706.4	705367.6	17.1	7.2	5.5	5.5	*	Grouler Contact (Probable Bupy Mooning)	M49, NS0
CB		-81.8004522	433291.6	4605702.6	2159819.9	705230.1	17.1	44.3	1.0	1.5	D.1	Rectangular Contact	141
C11		-81.7942784 -81.7802254	433806.A 434970.8	4605574.0 4604611.5	2161527.9 2165992.0	704189.5 701744.9	16.9	79.4 175.5	3.2	0.3	0.2	Linear Contact Linear Contact	
C13		-81.7733918 -81.7591219		4604351.Z 4603848.3	2167268.2 2171185.5	700923.0 699340.0	16.0 15.8	125,8 15.1	3.5 5.7	0.9	0.2	Rectangular Contact Linear Contact	
CIA	41.5031114	7.7.2.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.		4603766.6	2172256.9	699090.4	36.4	102.6	19.5	8.6		Circular Contact (Possible	
-							15,5757		01/2/2		22.22	Dredge Spoil) Low Reflectivity Patch (Possible	- 63
C15	41.5801031	-81.7460655	437807.9	4603426.2	2174769.0	698016.5	- 1	177.1	3.9	2.4		Slag	
C16	41.5785477	-81.7451360	497883.9	4603252,6	2175028.2	697451.3	15.9	62.8	8.1.	1.4	D.6	Loss Reflectivity Patch (Possible Slag)	1.5
C17	41.5794293	-81.7450774	437889.6	4603850.5	2175041,4	697772.6	15.9	150.9	11.0	0.4	0.0	Linear Contact	5 (#)
CIR	41.5782747		437896.6	4603222.2	2175071.0	697352.2	15.8	42.5	6.7	1.5	0.5	Low Reflectivity Patch (Possible Slag)	- 23
C19	41.5761775		437994.6 437940.0	4603193.6 4602989.0	2175197.3 2175290.0	697260.4 696589.1	15.9	36.0 139.4	1.2	0.5	- 400	Linear Contact Linear Contact	1 12
C21	41.5753894		70.00	4602900.7	2175549.6	696304.9	0.0	169.6	0.8	0.5	0.1	Circular Contact (Probable Tire)	1
C22	41.5749766	1000000	438144.3	4602853.5	2175905.2	696157.6	15.7	157.8	2.7	0.7	0.5	Point Source	
C23	41.5763451	-81.7416041	438176.2	4603005.6	2176001,5	696687.1	15.8	9.9	3.9	0.5	+.0	Linear Contact	
C25	41.5767962	-81.7412561 -81.7410623	438205.6 438222.6	4603048.7 4603149.4	2176095.4	696800.4 697131.6	15.8	130.2	9.2	0.2	0.1	Linear Contact Linear Contact	1 1
C26	41.5764126		100000000000000000000000000000000000000	4605012.4	2176246.2	696883.8	15.0	32.6	2.0	0.0	0.4	Low Reflectivity Patch (Possible	1 12
C27	41.5769110	-81.7405391	435255.5	4605067.6	2175291.0	896065.6	15.8	67.9	8.1	0.4	-	Stagi Linear Contact	
C28	41.5748567	81.7404957	438267.2	4602837.3	2176909.5	696110.1	15.7	112.2	2.8	0.6	0.1	Linear Contact	
C38	41.5759815		438291.5 438415.2	4603097.A 4602963.2	2176374.7 2176788.0	696565.1 696531.5	15.7	125.6 69.9	7.7	0.4	0.2	Linear Contact Linear Contact	-
C91		-81.7382422	438456.6	4603017.5	2176920.9	696712.2	15.7	137.6	11.1	0.3	0.1	Linear Cortact	
C32	41.5756655	-81.7376941	430501.5	4601927.3	2177073.4	696410.0	15.7	80.6	2.2	1.1	40	Low Reflectivity Patch (Possible Stag)	12
C33	41.5726019	-01.7357889	439657.A	4602585.9	2177604.4	693307.1	15.4	140.0	4.9	1.4	*	Circular Contact	9.
C34	41.5727777	-81.7355758	438675.4	4602605.2	2177662.2	695371.7	15.4	115.2	2.4	2.2	0.7	Circular Contact (Probable Oredge Spoil)	12
C35	41.5731210	-81.7352714	438701.1	4602643.1	2177744.4	695497.5	15.4	69.6	6.0	3.4	- 11	Rectangular Contact	(+)
Cal	41.5746957	-91.7351299	438714.3	4602811.2	2177778.2	696049.7	15.6	85.5	1.9	1.1	**	Loss Reflectivity Patch (Possible Slag)	(4)
C37	41.5742500	-91.7351027	439716.2	4602769.3	2177796.9	695909.3	15.6	47.1	2.1	1.5	1.0	Circular Contact	(the
CSE	41.5745852	-61.7350109	438724.2	4602805.5	2177011.0	696031.6	15.6	83,4	4.5	2.9	+-	Low Reflectivity Patch (Possible Slag)	
C39	41.5732856	-81.7349705	438726.3	4602661.2	2177826.2	693558.2	15.4	41.5	4.5	31	4895	Low Reflectivity Patch (Possible	12
_		4		-			-					Slag) Low Reflectivity Patch (Possible	
Cas	41.5720940	-81.7341911	438790.2	4602528.3	2178043.2	695125.9	35.8	126.2	7.0	5.6	*30	Slag)	
CHI	41.5749022	-01.7341269	430790.1	4602929.9	2179052.1	696112.0	15.6	140.0	2.6	1.5	D.B	Point Source (Probable Boulder)	(#)
042	41.5717875	-81.7540750	458799,7	4602494.2	2178076.5	693014.5	15.2	151.1	7.3	3.4	A 2	Low Reflectivity Patch (Possible	18
C43	41.5719459	-81.7940639	438800.7	4602511.8	2178078.5	695072.2	15.3	135.5	3.7	3.1	400	Stag Low Reflectivity Patch (Possible	
CHS	41.0/19439	91./940100	+3000077	+002512.0	21/80/652	600012.2	30.0	1999	317	2.1	***	Stag	
C44	41,5721798	-81,7336485	438835,5	4602537.5	2178191.4	695158.5	15.3	96.8	17.9	17,4	*33	Low Reflectivity Patch (Possible Stag)	
C45	41.5722820	-81.7332410	438869.6	4602548.5	2178902.6	695196.7	15.2	69.7	4.0	0.4	0.1	Linear Contact	100
C46	41.5729978	-81.7850702	430004.5	4602627.9	2178947.0	895457.8	15.4	6.0	2.0	0.4	0.5	Point Source (Probable Boulder)	18
047	41.5727958	61.7330514	438805,9	4602505.4	2178952.0	595384.3	15.5	12.1	1.3	1.0	0.5	Potrt Source (Probable Boulder)	191
C48	41.5726638	-81.7321082	438964,4	4603590.1	2170611.3	695338.5	15.3	12.9	1.2	0.9	0.7	Point Source (Probable	
200	200000000000000000000000000000000000000			1220000000000				135-139900				Boulder) Low Reflectivity Patch (Possible)	
C49	41.5726909	-81.7312521	439005.8	4602592.5	2178945.5	695350.5	15.3	49.9	2.6	1.2	0.3	Sing	3 75
C50	41.5719909	-01.7311854	439040,7	4602514,7	2170866.0	695093.6	15.2	15.6	AA	2.2	*	Low Reflectivity Patch (Possible Stag)	
C51		-81.7305695	439091.8	4602488.8	2179035.2	695013.4	15.2	13.2	1.9	0.5	0.3	Linear Contact	
C53		-81.7305075 -81.7300563	439095,6	4602526.1 4602527.5	2179056.9	694479.6 694486.3	15.5 15.3	155.5 135.3	3.6	0.5	0.0	Linear Contact Linear Contact	
		-81.7300EE3		4602270.4	2179173.2	694298.9		185.0	13.8	6.7	+-	Unknown Contact	
CSS	41.5711445	-81.7291570	439209.0	4602419.4	2179423.7	694792.1	15.3	16.5	4.0	1.7	100	Low Reflectivity Patch (Poscible Stag)	1 1
C56	41.5711069	-61.7291492	459209.6	4602415.2	2179426.0	594775.4	15.5	19.9	2.5	1.6	+//	Low Reflectivity Patch (Possible	+:
							72.77	100000	-		-	Stag) Low Reflectivity Patch (Possible)	(3)
C57	41.5711870	-81.7291293	499211.3	4602424.1	2179431.2	894807.6	15.5	11.3	1.7	2.5	*	Sing)	
CSE	41.5710575	-81.7290973	439213.9	4603409.6	2179440.8	694760.5	15.3	32.6	2,1	1.7	7.1	Low Reflectivity Patch (Possible Slag)	
C59	41.5712076	-91.7290676	439216.5	4603426.3	2179448.0	694815.3	15.3	6.8	6.1	3.6		Loss Reflectivity Patch (Fossible	7.5
C90	1777	-01.7297678		4602420.3	2179524.7	694796.8	15.3	0.7	3.1	0.6	D.2	Slag Linear Contact	
C61	41.5696265	-61.7204158	439269.6	4602272.5	2179630.0	694313.0	15.2	115.0	4.1	0.4	0.1	Linear Contact	14
C62	41.5706782	-81.7284075 -81.7283231	439271.0 439276.8	4602367.1 4602214.2	2179630.3 2179657.8	694624.0 694122.8	15.2	162.4	3.3	0.6	D.4 D.3	Linear Contact Linear Contact	F/892
C64		-81.7283218	499277.2	4602255.4	2179657.0	694258.0	15.2	125.6	1.5	0.5	0.1	Linear Contact	
C65	41.5706138	-81.7282609	439283.3	4600359.8	2179670.8	694600.9	15.3	32.2	3.4	1.0	77.5	Low Reflectivity Patch (Possible Slag)	9
CG5		-81.7292402		4602270.0	2179679.9	694302.7	15.2	109.4	1.9	0.5	- 86	Linear Contact	18
C67		-01.7202310	439296.2	4603424.3	2179676.7	694012.6	15.3	25.5	3.3	0.0	D.4	Linear Contact Low Reflectivity Patch (Possible	
C68	41.5707968	-61.7262010	439288,3	4602573.4	2179686.6	694645.6	15.2	17.9	5.2	1.5	- 100	Slag	
		-81,7281394	439293,3	4602360.1	2179703.8	694602.4	15.2	27.0	8.5	3.5	+	Low Reflectivity Patch (Possible	0 9

95	MADES 6	ieographic	NADES S	ITM Zone 17	WADER ONE S	Side tate Plane florth	can Sonar Con					12	
10	Lattindo	Longitude	East (re)	North (m)	East(US servey feet)	North (US servey feet)	Bathyreetry (m)	Distance from Proposed Route (ne)	Length (m)	Width (m)	Height (m)	Description	Associated Mag Anomaly ID
C70	41.5705235	-81.7280796	439298.2	4602349.5	2179720.5	694568.0	15.2	33.8	3.0	0.7		Low Reflectivity Patch (Possible Stag)	200
C71	41.5701074	-81.7280231	439302.6	4602303.4	2179797.3	694416.9	15.2	72.0	4.2	2.8	0.1	Grouler Contact Low Reflectivity Patch (Possisle	(4)
C72	41.5705831	7.02		4602356-2	2179741.7	694590.3	15.2	24.8	2.6	2.1	-	Slag	
cm.		-81 7279966		4602308.3	2179744.4	694434.8	15.2	66.1	4.2	1.8	-	Orcular Contact Low Reflectivity Patch (Possible)	
L74	41.5702992	-81.7279554	439310.0	4802324.7	2179760.7	694487.0	15.2	49.8	2.5	1.6	-	Sing)	
ETS.	41.5709050	-81.7276572	430335.6	4602525.2	2179782.1	694489.5	15.2	45.1	5.D	1.5		Low Reflectivity Patch (Possible Skeg)	
C76	41.5702668	41.7276261	499319.1	4602323.0	2179790.7	694475.5	15.2	48.5	4.2	1.0		Low Reflectivity Patch (Possible Sleg)	
C77	41.5713950	41.7277941	439323.8	4682567.2	2179792.6	695251.0	15.2	159.9	2.8	1.6	12	Low Reflectivity Patch (Possible	-
C78	41.5691421	-81.7270113	439386.0	4602195.5	2180017.3	694057.7	15.1	125.3	3.3	0.4	0.0	Slag(Linear Contact	
C79 CB0	41.5694892	-81.7267636 -81.7264907	439432.0	4602333.9 4602506.4	2180083.9 2180150.7	69196.7 695990.2	15.1	81.6 168.4	3.1	1.1	1.0	Grovier Contact Grovier Contact	
CBI	41.5718742	100000000000000000000000000000000000000	439441.5	4603498.A	2180162.2	695064.7	15.3	166.1	7.2	4.1	1	Low Reflectivity Patch Possible	77.77
CB2	41.5710858		439442.7	4603430.9	2180391.3	694777.5	15.3	90.3	3.0	0.6	0.1	Stagi Linear Contact	M113, M214
085	41.5717858	41.7262595	499451.7	4602488.5	2180214.5	695032.7	15.5	162.2	9.1	LS		Low Reflectivity Patch (Possible	M82
(84	41.5707449	-81.7261001	499463.5	4602372.8	2180261.4	694653.7	15.2	67.2	2.8	1.8	0.6	Strg Point Source (Probable	13.
100	41.0101443	41.7261001				004033.7	19-4	AL-T	2.0	Te	0.6	Soulder) Low Reflectivity Patch (Possible)	
085	41.5714122	-81.7260088	489471.7	4603446.9	2180284.3	694897.2	15.2	135.9	13.6	4.2	. 22	Slag)	M215
CBS	41.5714945	-81.7259549	439475.5	4603456.0	2180298.9	694927.4	15.2	146.1	6.7	4.9	.6	Low Reflectivity Patch (Possible Step)	W216
087	41.5709615		639679.7	4602396.8	2180913.3	694733.3	15.2	95.1	10.1	0.5	0.1	Linear Contact	N/112
CEG	41.5705741	-41.7254051	439521.3	4602353.6	2180452.2	694593.3	15.2	78.5	9.5	0.5	0.2	Linear Contact Low Reflectivity Patch (Possible	-
C89	41.5702816	-81.7252589	439533.2	4602320.8	2180493.1	694487.1	15.1	56.0	11.2	4.0	-	Slag Low Reflectivity Patch (Possible)	
C90	41.5704508	-81.7251787	439540.0	4602339.5	2180514.5	694549.0	15.1	75.6	13.0	5.1	- 00	Slag)	1000
091	41.5703843	-81.7251217	498544.7	4602332.1	2180530.9	694524.9	15.1	71.5	4.9	1.1		Low Reflectivity Patch (Possible Sleg)	7.85
092	41.5701709	-81.7245097	499595.6	4602307.9	2180696.7	694448.4	15.0	75.2	13.4	7.5	-	Lew Reflectivity Patch (Pomisie	124
			L		Constant			2	_		2400	Stag) Low Reflectivity Patch (Possible	
C93	41.5697449	-91.7248667	439598.7	4602260.6	2180711.6	694293.4	16.0	35.5	6.1	2.5	0.6	Steg	
194	41.5695610	-01.7244551	439599.5	4602240.3	2180715.4	694226.5	14.9	10.1	6.2	2.8	194	Low Reflectivity Patch (Possible Slag)	3.00
C95	41.5689934	41,7244120	439601.7	4602077.3	2180731.9	693691.9	15.1	125.0	1.5	14	0.6	Point Source (Probable Boulder)	(4)
C96		-81.7243582	439606.1	4602063.5	2180747.0	693647.0	15.1	132.9	5.4	0.5	0.1	Linear Contact	1.4
C57	41.5679357		439611.1 439632.9	4602059.6 4602064.3	2180788.5 2180835.0	693634.5 693651.1	15.1	155.8	4.9	0.5	0.2	Linear Contact Linear Contact	(2) TeV
(99	41.5691417		439639.6	4602199.4	2180845.5	694074.9	14.5	3,3	6.6	5.9		Linear Contact	-
1.00	41.5691421	-81,7270113	439385.0	4802385.5	2180017.3	694067.7	15.1	125.3	3.5	0.9	0.4	Linear Contact	
101	41.5679910	7.75	439656.5	4602092.1	2180914.2 2180913.4	698546.9 694181.5	15.0	135.6	2.6	2.5	0.3	Linear Centact Low Reflectivity Patch (Possible)	MISS
103		-81,7296402	439666.0	4602059.8	2100943.6	690638.1	15.0	106.9	4.2	0.3	0.0	Slag Linear Contact	Witten
104	41.5691001		439670.6	4602197.4	2180951.0	694089.0	14.9	15.4	4.9	3.1	1	Low Reflectivity Patch (Possible	
_			-				15000					Slag Point Source (Probable	
1.05	41.5692913	41.7235862	439671.7	4602209.7	2180954,0	694130.3	14.5	26.7	2.8	0.9	0.7	(Soulder)	(*)
106	41.5692118	41.7294997	439678.9	4502206.8	2180977.9	694101.6	14.9	22.5	1.8	1.0	0.5	Point Source (Probable Soulder)	((*))
1.07	41.5691907	-81.7234616	439682.0	4602185.1	2180988.5	694083.1	14.9	19.0	8.8	23.	0.8	Low Reflectivity Patch (Possisle	(F)
1.00	41.5688718	-81,7233361	499992.2	4602369.0	2181023.8	693978.1	15.0	4.1	4.0	0.5	0.1	Stag) Linear Contact	
109	41.5694729	41.7252421	439700.6	4602229.6	2383047.6	694197.4	14.9	51.2	2.1	1.0	0.2	Point Source (Proteable Soulder)	100
130	41.5684564	-81.7291099	499750.7	4602136.7	2181087.3	693927.3	15.0	35.4	3.0	0.7	0.1	Linear Contact	
111	41.5689415	-01.7231011	439711.0	4602170.5	2183087.9	694006.1	15.0	12.1	2.3	0.4	0.3	Linear Contact	
112	41.5675506	-81.7224855	499762.0	4602036.6	2181261.4	693591.7	14.8	97.6	4.6	5.0		Low Reflectivity Patch Possible Slag	
113	41.5685835	41.7224107	439769.2	4602141.4	2181277/6	693911.8	15.0	14.8	3.8	1.7		Low Reflectivity Patch (Possible	100
114	41.5682369	-81.7223625	489773.2	4602146.1	2181290.7	698927.5	15.0	20.9	3.8	1.1	-	Slag Low Reflectivity Patch (Possisle	
-		200000000000000000000000000000000000000	The contract			7.0000000000000000000000000000000000000	10000					Sleg) Point Source (Prohable	-
115	41.5681048	-81.7222909	439778.6	4602077.0	2181312.3	699701.0	14.8	36.8	2.8	0.7	1.0	(Soukler)	223
116	41.5685281	-81.7222826	639779.7	4602124.1	2181313.2	603255.4	14.0	4.0	4.6	1.9		Low Reflectivity Patch (Possisle Slag)	2.5
		-01.7222544	439782.2	4602343.2	2183320.3	693916.4	14.9	22.7	7.4	1.5	0.2	Low Reflectivity Patch (Possible	140
117	41.5607000		10000000000	100000000000000000000000000000000000000		100000000000000000000000000000000000000	X37539	250.00	-	1.5	0.3	Stag! Low Reflectivity Patch (Possible	
117			current o	20020007	******	600 No. 2	12.0	16.6					250
117	43.5682772	-81.7222051		4602096.2	2181335.2	693764.2	14.8	16.5	3.6	- 115		Slag	
117	43.5682772 43.5683570	-81 7221051 -81 7221252	499792.7	4602105.0	2181356.8	693793.5	14.9	5.6	9.1	3.4		Stag Low Reflectivity Petch (Possible Stag	
117	41 5682772 41 5683570 41 5683688	-81 7222051 -81 7221252 -81 7220727	499792.7 499797.0	4602105.0 4602085.1	2181356.8 2181371.5	695793.5 695761.5	14.9	5.6 12.0	9.1	3.4	0.2	Low Reflectivity Petch (Possible Slag) Linear Contact	
117	41 5682772 41 5683570 41 5683688	-81 7221051 -81 7221252	499792.7 499797.0	4602105.0	2181356.8	693793.5	14.9	5.6	9.1	3.4		Low Reflectivity Patch (Possible Slag) Linear Contact Low Reflectivity Patch (Possible Slag)	M156
117	41.5682772 41.5683570 41.5682688 41.5686324	-81 7222051 -81 7221252 -81 7220727	439792.7 439797.0 439797.4	4602105.0 4602085.1	2181356.8 2181371.5	695793.5 695761.5	14.9	5.6 12.0	9.1	3.4	0.2	Low Reflectivity Patch (Possible Slag) Linear Contact Low Reflectivity Patch (Possible Slag) Low Reflectivity Patch (Possible	-
117	41.5682772 41.5683570 41.5682688 41.5686324 41.5696837	-81 7222051 -81 7221252 -81 7220727 -81 7220719 -81 7219585	499792.7 499797.0 499797.4 499907.0	4602105.0 4602105.1 4602135.5	2181356.8 2181371.5 2181370.5 2181398.1	695793.5 695761.5 693894.0	14.9 14.8 14.9	5.6 12.0 23.4 139.9	9.1 4.1 4.0 12.2	3.4 0.6 2.5	0.2	Low Reflectivity Patch (Possible Slag) Linear Contact Low Reflectivity Patch (Possible Slag) Low Reflectivity Patch (Possible Slag) Low Reflectivity Patch (Possible Low Reflectivity Patch (Possible	M156
1127 1128 1129 1123 1122	41 5682772 41 5683570 41 5683688 41 5686324 41 5696807 41 5603659	-81 7221051 -81 7221252 -81 7220727 -81 7220719 -81 7219585 -91 7219549	439792.7 439797.0 439797.4 439907.8 439908.5	4602105.0 4602095.1 4602195.5 4602253.0 4602253.0	2181356.8 2181371.5 2181370.5 2181396.1 2181408.9	695793.5 695761.5 695894.0 694276.2 695797.2	14.9 14.8 14.9 14.9	5.6 12.0 23.4 139.9 3.0	9.1 4.1 4.0 12.2	3.4 0.6 2.5 10.8	0.2	Low Reflectivity Patch (Possible Step) Linear Contact Low Reflectivity Patch (Possible Step) Low Reflectivity Patch (Possible Step) Low Reflectivity Patch (Possible Step)	MIS6
117 118 119 120 121 122	41.5682772 41.5683570 41.5685888 41.5686324 41.5696807 42.5603659	-81 7222051 -81 7221252 -81 7220727 -81 7220719 -81 7219585 -91 7219549 -81 7217073	499792.7 499797.0 439797.4 439907.8 439907.5 439627.6	4602105.0 4602105.1 4602105.5 4602251.9 4602251.9 4602250.2	2181356.8 2181371.5 2181370.5 2181390.1 2181400.9 2181470.8	695793.5 695761.5 699894.0 694276.2 695797.2	14.9 14.8 14.9	5.6 12.0 23.4 129.9 3.0 21.3	9.1 4.1 4.0 12.2 1.2	3.4 0.6 2.5 10.8 1.1	0.2	Low Reflectivity Petch (Possible Step) Livear Cerebest Low Reflectivity Patch (Possible Step) Low Reflectivity Patch (Possible Step) Low Reflectivity Patch (Possible Step) Point Source (Probable Goulder)	M156
117 118 119 120 121 122 123	41 568 2772 41 568 3570 41 568 2688 41 568 6324 41 568 6324 41 568 6324 41 568 6324 41 568 6324 41 568 6324	-81 7222051 -81 7221252 -81 7230727 -81 7230719 -81 7219585 -81 7219596 -81 7217073 -81 7217073	499792.7 439797.0 439797.4 439807.0 439807.0 439827.6 439827.6	4602105.0 4602105.1 4602105.1 4602251.9 4602251.9 4602105.0 4602106.2	2181356.8 2181371.5 2181370.5 2181366.1 2181466.9 2181470.8 2181520.2	693793.5 693761.5 693894.0 694276.2 693797.2 693832.4	14.9 14.8 14.9 14.0 14.0	56 120 234 1299 30 213 2633	9.1 4.1 4.0 12.2 1.2 1.7 2.8	3.4 0.6 2.5 10.8 3.1 1.0	1.0	Low Reflectivity Petch (Possible Skel) Lorent Centect Low Reflectivity Patch (Possible Skel) Low Reflectivity Patch (Possible Skel) Low Reflectivity Patch (Possible Skel) Point Source (Probable Goulder) Rechangular Contact	M211
1117	41.5682772 41.5683570 41.5685888 41.5686324 41.5696807 42.5603659	-81 7222051 -81 7221252 -81 7230727 -81 7230719 -81 7219585 -81 7219596 -81 7217073 -81 7215961	499792.7 439797.0 439797.4 439807.0 439807.0 439827.6 439827.6	4602105.0 4602105.1 4602105.5 4602251.9 4602251.9 4602250.2	2181356.8 2181371.5 2181370.5 2181390.1 2181400.9 2181470.8	695793.5 695761.5 699894.0 694276.2 695797.2	14.9 14.8 14.9 14.9	5.6 12.0 23.4 129.9 3.0 21.3	9.1 4.1 4.0 12.2 1.2	3.4 0.6 2.5 10.8 1.1	0.2	Low Reflectivity Petch (Possible Stag) Linear Contact Low Reflectivity Petch (Possible Stag) Low Reflectivity Petch (Possible Stag) Low Reflectivity Petch (Possible Stag) Row Reflectivity	MISE -
-	41.5682773 41.5682588 41.5682588 41.5686324 41.5686327 41.5686329 41.5686329 41.5684611 41.5664987	-81 7222051 -81 7221252 -81 7230727 -81 7230719 -81 7219585 -81 7219596 -81 7217073 -81 7215961	439792.7 439797.0 439797.4 439907.8 439808.5 439827.6 439838.9 439841.6	4602105.0 4602105.1 4602105.1 4602251.9 4602251.9 4602105.0 4602106.2	2181356.8 2181371.5 2181370.5 2181366.1 2181466.9 2181470.8 2181520.2	693793.5 693761.5 693894.0 694276.2 693797.2 693832.4	14.9 14.8 14.9 14.0 14.0	56 120 234 1299 30 213 2633	9.1 4.1 4.0 12.2 1.2 1.7 2.8	3.4 0.6 2.5 10.8 3.1 1.0	1.0	Low Reflectivity Petch (Possible Stag) Linear Ceretars Low Reflectivity Petch (Possible Stag) Reflectivity Petch (Possible Souther) Rectangular Contact Point Source (Probable	M211
1117 1118 1128 1121 1122 1123 1123 1125 1127	41 568 2772 41 568 3570 41 568 5888 41 568 6824 41 568 6827 41 568 6827	-81 7222051 -81 7221252 -81 7220727 -81 7220719 -81 7219585 -81 7219548 -81 7217073 -81 7215501 -81 7215592	499792.7 499797.0 439797.4 439807.0 439807.5 439827.6 439835.9 439841.6	4602105.0 4602095.1 4602235.5 4602251.9 4602125.0 4602106.2 4602106.2 4602107.9	2181356.8 2181371.5 2101370.5 2101390.1 2101400.9 2101470.8 2101520.2 2181520.2	695793.5 695761.5 698994.0 694276.2 693797.2 693832.4 693117.8 693838.T	14.9 14.8 14.9 14.0 14.0 14.0	\$6 12.0 23.4 129.9 3.0 21.3 363.3 29.7	9.1 4.1 4.0 12.2 1.2 1.2 2.8 1.5	3.4 0.6 2.5 10.8 1.1 1.0 1.2	0.2 - - 1.0 1.1	Low Reflectivity Petch (Possible Ske) Linear Centect Low Reflectivity Patch (Possible Ske) Low Reflectivity Patch (Possible Ske) Low Reflectivity Patch (Possible Ske) Low Reflectivity Patch (Possible Sca) Roard Source (Probable Souther) Recta regular Contact Point Source (Probable Souther)	M211
1117 1118 1118 1120 1121 1122 1123 1125 1127	41.5682772 41.5683570 41.5684888 41.5684807 41.5684807 41.5684817 41.5684817 41.5684817 41.5684773 41.5684773	41.7221051 41.7221051 41.7210727 41.7210945 41.7210946 41.7217074 41.7217074 41.7215061	499792.7 499797.0 439797.4 439807.0 439807.5 439827.6 439835.9 439841.6	4602305.0 4602095.1 4602305.5 4602253.0 4602305.0 4602305.2 4602305.2 4602305.2	2181356.8 2181371.5 2181370.5 2181390.1 2181490.9 2181470.8 2181520.2 2181520.2	693793.5 693761.5 693894.0 694276.2 693797.2 693832.4 693838.7 693838.7	14.9 14.6 14.9 14.0 14.0 14.0 14.0	56 120 234 1399 3.0 21.5 263.3 29.7	9.1 4.1 4.0 12.2 1.2 1.2 2.8 1.5	3.4 0.6 2.5 10.8 1.1 1.0 1.2 1.5	0.2 - - 1.0 1.1 0.5	Low Reflectivity Petch (Possible Skej) Liveur Ceretars Low Reflectivity Patch (Possible Skej) Rechargular Cortact Posit Source (Probable Boulder) Point Source (Probable Boulder) Point Source (Probable Boulder) Roint Source (Probable Boulder)	M156

72	NADE2 G	ieographic	MADES U	TM Zone 17	NADBI ONE S	Side tate Plane frorth	can Senar Cen	Distance from					**************************************
10	Latitude	Longitude	East (m)	North (m)	East (US servey feet)	North (US servey foot)	Bathyreetry (m)	Proposed Route (ne)	(m)	(m)	(m)	Description	Associated Mag Anomaly ID
C132	41.5659769	-81.7201452	439955.5	4603839.3	2181906.4	692931.1	14.6	157.7	8.2	5.7		Low Reflectivity Patch (Possible Slag)	7350
CF39		-81.7201278	439959.5	4802343.4	2183902.3	699922.6	14.8	107.8	2.4	1.2	1.0	Rectangular Contact Point Source (Probable	
CL34	41.5676314	-41.7200550	439954.6	4602023.0	2183925.6	699534.2	14.8	7.0	2.0	0.6	0.5	Boulder)	
CI 35	41.5676987	-01.7197246	419992.2	4802030.2	2182015.8	699559.5	14.9	26.8	1.7	2.1	-	Low Reflectivity Patch (Possible Slag)	
C138	41.5675315	-81.7196271	440000.2	4602001.5	2382643:1	693498.7	14.8	14.4	2.1	1.1	0.6	Point Source (Probable Soulder)	
C137	110000000000000000000000000000000000000	-81.7156209	440000.0	4601928.5	2182647,2	693226.1	14.8	58.2	3.7	0.9		Linear Contact Low Reflectivity Patch Possible	M152
CLSE	41.5676191	81.7195825	440004.0	4602021.3	2182055.0	695530.8	14.8	24.7	6.5	4,5		Sleg	M158
C139	41.9674205	2000	440007.9	4601599.2	2182069.1	699458.6	14.8	7.4	2.5	1.7	-	Low Reflectivity Patch (Possible Slag)	-
			440013.2 440025.4	4602169.6	2182076.9	694018.2	14.8	158.7 35.4	3.6	0.4	0.5	Linear Contact Linear Contact	
		-81.7191049	440044.5	4602130.9	2182183.0	699827.9	14.9	122.8	3.5	0.4	1	Linear Contact	+
222	41.5673790	-81.7189203 -81.7183361	640059.0 440105.5	4601994.0 4601949.1	2192237.0	693464.6	14.0	27.8 75.4	4.0	0.6	0.1	Linear Contact Linear Contact	
-		-01.7161643	440112.9	4601898.8	2182419.3	693135.1	14.0	28.9	3.0	0.3	0.3	Linear Contact	
C146	41.5665197	81.7181509	440122.5	4601098.2	2162450.3	693133.8	14.8	24.8	1.0	0.8	0.6	Point Source (Probable Soulder)	
C147	41.5643678	-81.7171889	440200.5	4601658.6	2182720.6	692351.9	-	195.6	5.7	0.8	0.1	Linear Contect	
C1,48	41.5665584	-81,7147141	440408.7	4601877.9	2183391.3	695083.4	14.5	97.5	5.7	0.5		Linear Contact	
C1.45	41,5663363	2 (0.000,000)	440475.0	4601874.9	2183608.8	699077.4	14.4	127.2	6.8	0.2		Linear Contact Point Source (Prohable	
CF20	41,000,000	-81.7135349	440905.1	4603644,4	2189720.0	692322.6	14.2	59.1	4.0	0.9	0.3	(Novikler)	
C152	41.5654100	-81.7130571 -81.7120650	440529.0 440628.0	4803773.6	2189799.1 2184119.2	69274L5 692758.7	14.4	63.7 1154	10.6	3.1	0.1	Linear Contact Low Reflectivity Patch (Possisle	
							90.00	2000		20.22	7.00	Slag Point Source (Probable	2 2 2
C153	41.5652723	-81.7120203	440632.3	A601755.5	2184152.0	692694.4	14.4	100.0	1.6	1.5	0.9	Soulder)	7.00
C154	41.5650956	-81.7119548	440637.6	4601735.8	2184150.5	692630.1	14.4	85.4	1.4	0.8	0.7	Point Source (Probable Soulder)	100
C155		-81.7115199	440687.9	4603434.4	2184333.8 2184354.9	691578.1 692089.7		170.5	2.4	0.6	0.2	Linear Contact	
CL56	41.5636074	-81.7112257 -81.7111407	440997.1 440705.0	4601570.1 4601675.5	2184375.0	692436.0	14.5	90.1 65.7	8.0	0.5	0.1	Linear Contact Linear Contact	
C1.5#	41.5621918	-81.7108161	440729.9	4601412.6	2184471.7	691574.7	14.4	151.5	17.8	0.4	0.3	Linear Contact	
C159		-81.7104062 -81.7102922	440765.2	4601542.2 4601528.6	2184580.0 2184611.6	692001.9 691957.9	14.4	21.3	5.2	0.5	0.1	Linear Contact Linear Contact	
CLEA		-81.7101770	440788.2	0601525.2	2184643.2	691947.1	14.4	26.8	2.9	0.4	0.4	Linear Contact	-
C1 62	41.5641429	-81.7101760	440785.1	4803529.0	2104640.4	692287.4	14.5	64.1	1.3	4.0	0.5	Low Reflectivity Patch (Posside Stag)	3.43
C183	41,5636117	-81.7101548	440785.4	4001569.8	2184648.0	602093.9	14.4	13.5	1.2	11	0,6	Paint Source (Probable Soulder)	100
C164	41.5643818	-81.7101038	440791.3	4601655.3	2184659.4	692374.6	14.5	90.5	124	6.4	1.3	Low Reflectacty Petch (Possisle- Sleg)	1 980
C1 65	41.5645768	-81.7100824	440793.8	4601676.9	2184664.6	692445.6	14.5	110.1	4.8	2.6	38	Low Reflectivity Patch (Possible Slag)	1 1
C166	41.5647895	-81.7099927	440901.0	4601700.5	2384666.4	692523.5	14.5	134.6	10.4	4.3	-3	Low Reflectivity Patch (Possible Slag)	1.0
C167	41.5620329	-81.7098601	440909.5	4601354.4	2184783.8	691519.4	14.4	129.5	1.0	1.6	0.4	Point Source (Probable Boulder)	N144
CLSS	41.5635947	-01.7096064	440932.1	4601567.6	2194790.1	692029.1	14.4	22.7	2.7	0.6	0.1	Linear Contact	S 10+
		-01.7095612	440051,9	4601500.7	2104866.3	691903.6	14.4	6.3	5.D	0.5	0.6	Linear Contact	-
C170 C171	41.5625297	-81.7090747 -81.7090549	440875.4 440876.3	4601449.0 4601557.1	2184947.1 2184955.2	691702.4 691401.0	14.4	48.6 128.3	7.2	1.0	-	Linear Contact Linear Contact	-
C172	41.5627621	-81,7087721	447900.9	4603474.6	2185025.1	691787.8	14.4	13.9	7.5	0.6	0.2	Linear Contact	0.000
C1.73	41.5628261	-51.7081814	440941.9	4601481.3	2185365.2	691812.3	14.4	12.1	7.7	0.6	0.1	Linear Contact	
CL75		-81.7078989 -81.7065854	440974.3 441081.6	4601546.6 4601271.2	2185265.9 2185638.6	692028.4 691130.5	14.4	84.9 108.0	4.0	0.6	0.2	Linear Contact Linear Contact	
C176	41.5607966	-81 7061521	441117.6	4401254.6	2185753.6	691078.1	16.1	99.9	1.1	0.6	0.5	Point Source (Probable	140
C177	41.5610431	-81 7058256	441145.0	4601281.7	2185841.2	691168.9	16.0	62.8	1.0	0.4	0.1	Boulder) Linear Contact	
	TEST PARTIES	41.7057347	441152.6	4601282.7	2185866.0	691172.4	14.0	54.3	4.0	0.5	1	Linear Contact	- 1
C1.79	41.3611467	-81.7055942	441164.4	4601293.1	2185904.1	691207.1	14.0	43.4	2.5	0.7	0.0	Point Source (Probable Soulder)	
CLES	41.5605036	-81.7047237	441238.4	4601221.1	2186344.5	690975.0	14.0	71.0	1.4	0.9	0.6	Point Source (Probable Boulder)	200
CLEE	41.5604539	-81.7046716	441240.7	4601215.5	2186158.9	690957.0	13.9	75.8	2.2	1.1	0.4	Point Source (Probable Soulder)	((0))
C1 85	41.5600491	-81.7045812	441247.9	4601179.5	2186185.0	690809.7	13.0	109.5	1.1	0.7	0.5	Point Source (Proteable Soulder)	(#)
CLES	41.5597743	-81.7044097	441261.9	4901139.9	2186232.9	690710.0	13.9	129.4	0.0	0.6	0.5	Point Source (Probable Boulder)	1980
CLDS	41.5600965	-81.7036724	441324.4	4601264.0	2388430.9	691120.7	13.9	9.4	1.0	0.6	0.6	Point Source (Probable Boulder)	100
CLES	41.5618126	-81.7036052	441330.9	4001365.6	2186446.2	691434.7	13.9	101.3	1.0	0.7	0.0	Linear Contact	-
CLSS	41.5617893	-81.7035322	441336.9	4601363.0	2186466.3	691446.4	13.9	101.9	I.B	0.6	0.5	Point Source (Probable Soulder)	
CLET	41.5614265	-81.7083929	441348.2	4601322.6	2186505.6	691314.5	13.9	72.2	2.2	0.7	0.5	Point Source (Probable Soulder)	1888
C1.88	41.5614252	-81.7033161	441354.6	4601322.4	2186536.6	691314.3	13.8	75.2	1.6	0.9	0.6	Point Source (Probable Boulder)	8.0
C189	41.5592663	-81.7088146	441352.8	4601082.7	2186534.2	690527.6	13.6	134.8	1.1	0.7	0.6	Point Source (Proteable Boulder)	0.00
		-81.7006744		4601259.8	2187251.4	691121.2	13.3	137.9	2.3	0.4	0.2	Linear Contact	
C190		-81.7009e13	441903.2	4600977.6	2187962.0	690196.7	13.2	104.2	4.D	0.5	-	Linear Contact Point Source (Probable)	Q (1+). ()
		-81 6991500	441099.9	4803059.9	2187674.6	690472.3	13.2	1A.9	0.7	0.4	0.6	Boulder)	J.S.
C193	41.5590139	-81.6989471	441716.8	4601051.8	2187730.3	690446.6	13.3	16.0	12	0.7	0.6	Point Source (Probable Soulder)	
C154	41.5591477	-81.6605757	441764.5	4603066.2	2187886.3	690496.8	13.4	52.0	1.4	0.9	0.6	Point Source (Probable Soulder)	1050
0.36		-81.6979033		4600967,4	2388038.5	690174.7	13.5	15.4	1.0	0.7	0.5	Point Source (Probable Soulder)	37.
0.00		-81.6971195 -81.6964973	441866.7	4600751.5	2188236.5	689469.7	19.7	172.7	2.5	0.7	0.2	Linear Contact Point Source (Proleable	MIAN
CL97			441213.6	4600766.3	2188413.1	689521.5	13.2		2.1	1.4	0.6	Soulder) Point Source (Probable	1 2000
CLOS	41.5589094	-01.6962044	441935.2	4800971.1	2155451.4	690194.5	13.5	51.9	1.0	0.9	0.6	(loukler)	

						Side	scan Sonar Con	tacts					- 50
1.78	NADE3 6	ieographic	MADES U	TM Zone 37	NADBS ONE S	tate Plane North		Distance from					
10	Latitude	Longitude	East(m)	North (m)	East (US servey feet)	North (US servey feet)	Eathyreetry (m)	Proposed Route (ne)	(m)	(m)	(m)	Description	Associated Mag Anomaly ID
C199	41.5579418	-81.6960717	441955.6	4600990.8	2186520.8	690063.2	13.4	27.2	1.2	0.6	0.6	Point Source (Probable	
C200	41.5595616	-81 6059293	481968.1	4801010.6	2188557.4	690325.9	13.5	108.0	3.6	0.7	0.7	Boulder) Linear Contact	-
C507	1417344141		441978.7	4601011.0	2188592.1	690327.7	13.5	108.5	3.4	0.6	0.4	Linear Contact	-
C202	41.5560201	-01.6049755	482046.0	4800005.6	2188834.6	609657.4	13.1	37.9	7.2	1.7	0.2	Low Reflectivity Patch Possible	0
C200		-01.6947107	442068.2	4600629.3	2100096.4	609736.6	13.2	6.2	4.6	0.4		Steg Linear Contact	
		21010020					10000					Paint Source (Probable	
C204	41.5558011	-31.6946311	442059.6	4600682.2	2188908.6	689285.B	13.2	125.2	1.0	0.7	0.5	Soulder)	
C255			442085.0	4600741.9	2188956.2	689450.8	13.1	74.3	6.6	0.4	0.2	Linear Contact	
C206		-81.6925614	442248.0	4600056.2	2109402.4	609972.8	13.5	141.7	4.1	0.4	0.1	Linear Contact Point Source (Probable	
C257	41.5555337	-81.69(1.859	442277.5	4600660.8	2189592.6	689195.7	13.1	50.9	1.1	0.6	0.5	Boulder)	
	41.5571151		442284.0	4600836.4	2189603.9	689772.0	13.3	105.3	3.0	0.3	. +	Linear Contact	
C216	41,5569012	-81.6919940 -81.6919808	442294.8	4600768.1	2189643.4	689548.7 689728.7	18.2	99.5	4.1	0.4	-	Linear Contact	+
C233	41.5572323		442301.3	4600645.3	2129659.9	689728.7	13.2	125.0	3.2	0.1	100	Linear Contact Linear Contact	
C212	41.5562346	-81.6919059	662305.4	4600736.5	2189666.7	689451.7	13.2	28.5	6.1	0.5	0.2	Linear Contact	
C213	CONTRACTOR CONTRACTOR	THE RESERVE OF THE PERSON NAMED IN	442304.5	4600025.3	2109672.0	609736.0	13.2	105.7	2.6	0.5	0.3	Linear Contact	+
NAME OF TAXABLE PARTY.	41.5572423	-81.6917529 -81.6899398	442315.1 442464.0	4600650.3 4600659.0	2189705.2	609019.3	13.2	132.7	4.1	0.5	0.1	Linear Contact	
C215	41.5555181	-81.6898221	442474.6	4600657.5	2190237.2	689196.0	12.9	39.0 42.5	13.5	9.4	0.3	Linear Contact Linear Contact	
-			-		7005 7 157 15	77777777	737 127	-		-	-	Low Reflectivity Patch (Possible	
(21)	41.5552677	-81.6897696	442478.7	4600625.7	2190254.6	689104.9	12.9	20.2	14.5	7.4	0.7	Sing	
C218	41.5536396	-81.6895995	442/91.5	4500448.8	2190906.7	688512.1	12.8	131.3	1.1	0.5	0.5	Point Source (Probable	
C219	41.5562901	-81.6895567	442497.8	4600796.4	2190309.6	689456.1	12.9	522.4	7.8	0.8	0.1	Soulder) Linear Contact	
C555	41.5543942	-81,6090621	442536.9	4600532.3	2190451.2	688788.4	12.8	36.3	2.6	0.4	-	Linear Contact	+
C221	41.5563882	-81.6897626	442563.7	4600753.4	2190536.4	689515.7		169.7	4.5	0.4	0.3	Linear Contact	
C222	41.5532781	-01.6005019	442599.4	4606407.0	2190665.1	688383.7	12.6	114.4	1.0	0.7	0.6	Point Source (Probable	
C223	41.5526391	-61.6867105	442731.5	4600535.0	2191100.0	600154.9	12.6	112.6	E.9	0.7	0.2	Boulder) Linear Contact	
C224	41.5541710	-81.6866219	442740.2	4800505.9	2191119.8	660713.3	12.7	40.0	7.4	0.4	0.1	Linear Contact	
C225	41,5554069	-01.6864650	442752.6	4600426.9	2151165.1	688435.5	12.6	28.1	1.1	0.7	0.5	Point Source (Probable	
_			44Z%2.1					-				Boulderj	1474
CZ 26	0.000.000.0	-81.6865724		4600637.5	2191184.1	689146.6	12.7	188.6	19.6	0.9	0.2	Linear Contact Point Source (Probable	M75
C227	41.5517972	-81.6859713	442792.4	4600235.2	2191306.2	687828.2		170.6	1.8	0.9	0.5	Boukler)	
C228	41.5541670	-01 6050333	662797.7	0600505.0	2191306.3	688713.6	12.7	67.3	1.5	1.7	8.0	Point Source (Probable	1
			Vision of the								-	Boulder) Point Source (Probable	-
C229	41.5541516	-81.6058827	442901.9	4600503.2	2191312.2	688708.1	12.7	67.8	1.5	1.5	3.0	Goulderi	
C230	41.5527375	-01.6058030	442007.3	4600346.2	2191348.6	600193.1	12.6	66.5	6.D	0.3		Linear Contact	1.+.
C231	41.5539001	41.6857192	442815.5	4800475.2	2151367.8	500016.9	12.7	43.5	2.1	0.8	0.7	Paint Source (Probable	
-											-	Soutser) Point Source (Probable	
C232	41.5538888	41.6856907	442817.7	4600473.9	2151875.6	688612.9	12.7	50.0	1.5	0.8	0.6	Soulder)	7.45
C238	41.5540599	-81.6855265	442831.5	4600492.8	2150420.0	688675.6	12.7	73.2	3.6	0.2	0.1	Linear Contact	9-1-1-1
	41.5540713		442836.6	4900484.0	2191436.8	688679.9	12.7	76.8	2.4	0.5	0.1	Linear Contact	
		-81,6850973 -81,6848326	442868.0	4600586.7	2191534.6	688986.0 688575.0	12.6	178.0 73.8	2.6	0.5	0.2	Linear Contact Linear Contact	-
		-41.6846558	442903.5	4600416.6	2191660.6	669429.6	12.6	41.9	2.9	0.5	0.1	Linear Contact	-
		-81.6045677	442910.8	4600405.1	2191685.1	600392.3	12.5	35.4	4.5	0.5	0.2	Linear Contact	0.00
C239		-01.6045295	442934.5	4600479.3	2193699.3	609632 R	12.6	101.2	2.3	0.6	0.1	Linear Contact	0 (+)
C240		-01.6043472 -01.6043075	442930.3	4600544.0 4600485.9	2191741.1 2191753.6	600052.0 600050.0	12.6	366.9 316.9	2.5	0.5	0.1	Linear Contact Linear Contact	-
C242	CHARLES CONTRACTOR	-51.6841979	442942.2	4500480.6	2191784.0	608041.8	12.6	116.7	2.3	0.5	0.0	Linear Contact	-
C243		-81.6858111	442971.7		- Table 1			169.8	13.2	11.9	-	Circular Contact (Probable	M102
C043	41.3308331	-01-0030TFE	- MADELLE	4600135.6	2191900.4	687511.6	0.5	190.0	83.6	11.2	13	Oredge Spoil)	MUU.
C244	41.3521890	-81.683T990	442973.9	4600284.0	2191899-2	687998.4	32.4	39.4	2.4	0.9	0.5	Point Source (Probable Boalder)	
			Same				7000				_	Grouler Contact (Probable	
C245	41.5564578	-81.6964873	441919.6	4600796.3	2188412.1	689521.5	13.2	133.9	16.7		.65	Oredge Spoil)	1.00
	The second second	-81.6035536	442995.3	4800985.7	2191962.9	600365.2	12.4	68.5	2.4	0.5	0.3	Linear Contact	of state to
C247 C248	and the second second	-01.6894705 -01.6893425	449002.6 449013.5	4600443.9	2191984.2 2192018.2	600534.5	12.5	114.2	2.0	0.E 0.4	0.2	Linear Contact Linear Contact	-
	2000		1000				14.5				1.15.15	Point Source (Probable	
C249	1000	-81.6855227	449015,4	4600503.6	2190022.8	688721.4		172.5	1.5	1.1	0.5	Soulderj	
		-81.6851299			2192058.9	608111.5	12.4	15.2	6.D	0.2	18	Linear Contact	
_	-	-81.6831028		4500455.7	2192064.1	600598.2	12.4	147.3	3.0	0.5		Linear Contact Grouler Contact (Probable	
6255	41.5514445	-81.6829157	443046.9	4600200.7	2192143.5	687729.4	12.2	76.8	5.6	5.3	0.5	Credge Spoil)	MLS
C258	41.5514225	-81.6829723	449050.6	4600203.8	2192155.3	687789.7	12.2	71.8	4.6	5.1	0.5	Groviar Contact (Probable	9
	CO. 10 POSTS	PC000000000000000000000000000000000000	1 ROWSY CO.	- Annabad	200000000000000000000000000000000000000	3500000	2000	3,500	1			Overlige Spoils	J 64%
C254	41.5504814	-81.6827315	449051.4	4600053.7	2192197.2	607379.9	12.5	162.6	14.5	15.8	LD	Groular Contact (Probable Oredge Spoil)	*
					2182222	******						Point Source (Probable	
C255	41.5539100	-01.6026490	443071.3	4600474.9	2192206.0	600030.5	3	174.8	1.0	0.9	0.5	Boulder)	7.5
C256	41.5507157	-81.6825446	443077.2	4600119.6	2352247.5	687464.8	12.4	132.3	17.1	14.3	11	Omular Contact (Probable	M140
-				11177	200000000		355	1000	7500	3460	-	Oredge Spoil) Orcular Contact (Probable	77.00
C257	41.5510598	-81.6823615	443092.8	4600157.6	2192296.5	687590.6	12.5	91.5	15.9	14.6	0.6	Oredge Spoil)	ML3
C258	41.55 2-7	-91.6823186	449096.5	4600170.4	2192307.8	687632.6	12.4	78.6	14.0	13.7	0.8	Grouler Contact (Probable	1
1476	-4-0935747	-91.0012190	***************************************		E356501.4	00.032.0	164	14.0	14.0	15.7	4.6	Oredge Spoill	100
C259	41.5524078	-91.6822663	443101.9	4600907.2	2192317.9	699092.0	12.4	49.5	1.5	1.5	0.2	Growler Contact (Probable Tire)	650
C260	41.5501032	-81 6818880	449131.5	4600051.1	2192429.4	687243.3		564.9	3.0	1.6	0.3	Linear Contact	-
	7. 7.77	-01.6010519		4600273.0	2193452.4	607971.7	12.5	30.4	1.9	0.7	0.6	Point Source (Probable	3
		100000000000000000000000000000000000000	15/20/19/20	A 2000 PA 2000 C	12900000000	590038000	11.5	15.57	1000	-2327	1777	Goulder)	3.5
		-81.6814695 -81.6817669		4600434.9	2192583.1	600504.7	15.6	187.9	7.7	0.7	0.0	Linear Contact	Autor
		-81.6017669		4800033.7	2192596.9	607109.2	12.4	155.4		0.4	0.1	Linear Contact Point Source (Probable	M103
		-81.6809926	445207.5	4600220.1	2152665.2	687802.0	12.5	19.0	1.4	0.7	0.8	Soulder)	1.5
		41.6805545		4600222.2	2152789.0	687810.9	12.6	38.7	3.7	0.5	0.1	Linear Contact	100
		-81.6799997		4600334.5	2192936.0	688116.6	12.5	142.3	3.3	0.5	0.4	Linear Contact	
(267	100000000	-81.6798199	700000	4599970.4	2192995.1	686988.1	12.4	152.8	2.0	1.5	-	Rectangular Contact Point Source (Probable	-
		-81.6796207	443321.3	4600141.7	2199647.1	687551.3	12.4	4.3	1.6	0.7	0.6	Boulders	150
C269	41.5516782	-81,6795035	443331.7	4600224.4	2199076.6	687823.3	12.4	83.5	3.2	0.3	0.1	Linear Contact	- (e)
C270	41.5521062	-01.6794338	441138.0	4800280.8	2190090.9	600000.5	12.5	1158	1.2	1.2	0.7	Point Source (Probable	
		0.0000000000000000000000000000000000000	100000000000000000000000000000000000000		A		7.55	N. A. A. C. C.				(Soulder)	

						Side	scan Sonar Con	tacts					- 93
	MADES G	eographic	MADES 1	ITM Zone 37	NADBS ONLY S	tate Plane forth		Distance from		Width		The same second	Associated Mag
10	Latitude	Longitude	East (m)	North (m)	East (US servey feet)	North (US servey feet)	Bathymetry (m)	Proposed Houte (ne)	(m)	(m)	(m)	Description	Anomaly ID
C273	41,5510600	-81.6787136	443397,0	4600155.3	2199294.9	687600.1	12.6	85.1	1.7	0.6	0.6	Point Source (Probable Boulder)	
0272	41.5515349	-81.6762774	643433.8	4600207.7	2199412.7	687774.2	12.5	118.9	1.7	0.6	0.6	Point Source (Probable	
C273		-81.6781199		4900154.2	2193456.5	687599.4	12.6	78.6	12.2	0.9	0.2	Boulder) Linear Contact	
C274		-81.6779915		4600040.3	2193496.1	607225.3	12.4	16.1	4.1	0.7	0.6	Linear Contact	3.40
C275	41.5511725	-81.5779343	445452.1	4500157.2	2193507.8	687643.0	12.6	97.4	1.0	0.7	0.6	Point Source (Probable Boulder)	(e)
0278	41.5518635	-81.6776264	443455.4	4900243.8	2199589.7	667695.6		177.0	1.5	1.0	0.7	Point Source (Probable Boulder)	
5277	41.5519197	81.6775816	443492.2	4600250.0	2159601.8	687916.2	-	184.3	1.4	1.2	0.6	Point Source (Probable	
C278	41.5507812	-81.6770972	443531.6	4600123.2	2158738.3	687502.6	12.5	93.0	3.3	0.2	0.1	Boulder) Linear Contact	
C279	41.5510166	-81.6769191	449546.7	4600049.3	2159786.2	687588.9	12.6	123.0	7.4	0.2	+	Linear Contact	
CSB	41.5510285		443552.8	4599637.6	2199806.2 2199880.2	687593.4 686568.0	12.6	127.1	3.3	15.9	0.5	Linear Contact Groular Contact (Probable	
CHI		-81.6766111	663509.9	4599637.8	2199890.2	606568.0	12.3	100.7	5.6	15.9	0.6	Oredge Spoil) Linear Contact	-
C282	41.5454096		441590.3	4399627.8 4399668.A	2190945.5	600003.6	11.0	95.9	13.0	15.1	0.4	Ontular Contact (Probable	
-								-	-			Oredge Spoil) Ortular Contact (Probable	
C283	41.5484909	110000000000000000000000000000000000000	443593.7	4599068.5	2199956.4	686670.1	12.5	107.0	19.6	17.3	1.5	Oredge Spoil)	
C284	41,5508066	41.6763271	443595.7	4600103.4	2199949.7	687441.0	12.5	9L3	4.2	0.5	0.2	Linear Contact Circular Contact (Probable	
CSB2	42.5489524		443597.2	4599675.3	2199967.7	686692.7	12.5	136.0	11.9	15:9	0.6	Ovedge Spoil)	M34, M38
CSR	41,5508125	-81.6760986 -81.6760747	443614.9	4600126.1	2194011.5	687516.6	11.0	70.4	5.7	0.3		Linear Contact Croular Contact (Probable	ALL PER
C287	41.5495795	-81.6760747	443615.1	4599889.2	2104025.4	696739.5	11.5	60.5	14.6	16.9	0.7	Oredge Spoil)	MISS
C288	41.5487472	-81.6750931	443621.9	4599696.7	2194047.5	606764.4	11.5	43.6	17.3	18.4	1.1	Circular Contact (Probable Oredge Spoil)	M200
C289	41.5489684	-81.6758657	443632.6	45999000.1	2154061.9	686838.9	12.0	245.8	14.7	10.0	0.7	Ortular Contact (Probable	
C250	41.5463369	-81 6747615	443722.5	4599628.3	2194392.9	685889.4	12.4	155.2	0.9	0.7	0.7	Oradga Spoil) Point Source (Probable	120
C291	41.5504215			4600081.7	2154401.7	687377.8	11.5	216.3	4.4	0.3	47	Soulder) Linear Contact	
C292	41.5465075	81.6744406	443749.5	4599647.0	2154480.2	605952.4	12.1	229.3	15.9	1.1	0.4	Linear Contact	
C299	41,5461014	-81.6797736	443904.7	4599601.5	2194664.1	685806.L	12.4	132.8	1.1	0.8	0.5	Point Source (Probable Soukler)	34.
C2 84	41.5497934	-81 6736843	443815.4	4600009.9	2194675.9	687146.0	-	544.0	1.0	0.6	3.0	Point Source (Probable	100
C295	41.5425973	-81.6795217		4599212.3	2194745.2	694530.0	12.2	209.7	1.1	0.6	1.0	Boulder) Point Source	
C296		-81.6735/062		4599612.7	2194798.4	605844.0	12.0	224.8	1.0	1.1	0.9	Point Source (Probable	-
C297	100000000000000000000000000000000000000	-61.6724721	TARGET STATE	4399546.6	2155022.1	605631.9	12.0	226.7	1.5	0.9	0.1	Boulder) Linear Contact	
C256	41.5455854	-81.6724516	443934.5	4599543.4	2199017.8	685621.5	12.2	111.3	3.0	0.6	0.2	Linear Contact	195
C286	41,5466707	V	449935.7	4599663.7	2199090.2	686017.6	12.1	10.8	3.4	0.8	0.4	Linear Contact Point Source (Probable	
		-81 6719941		4599792.8	2195145.2	686442,4	12.2	126.5	1.3	0.8	0.6	Soulder)	0.907
C810	41.5499411	-81.6715992 -81.6715162	443956.1 443993.7	4599691.2	2195342.4 2195279.2	686111.2	12.2	59.0 69.1	3.9	0.3	0.5	Linear Contact Linear Contact	-
C303	41,5466534	-01.6711224	444036.5	4599661.6	2195387.9	686016.0	11.2	533.2	1.0	0.0	0.5	Point Source (Prollable Boulder)	
			-44466600					Partie.					
C314	41.5403643	-81.6710955	444023.1	4596962.8	2195417.1	643722.7	11.3	105.6	2.6	4.1	0.9	Point Source	
C314		-81.6710955 -81.6707211	444073.1 444055.0						2.6	4.1 1.9	0.9	Point Source Linear Contact	
22.5	41.5621899		444023.1	4596962.8	2195417.1	683722.7	11.3	105.6	2.6			Point Source Linear Contact Point Source (Probable Boulder)	-
C905	41,5471899	-81.6707211	464023.1 464056.0 464061.9	4596962.8 4599165.3	2195417.1 2195513.2	623722.7 604388.9	11.3 12.1	385.6 32.3	2.6	1.9	-	Point Source Linear Contact Point Source (Probable Boulder) Point Source (Probable	
CSDS CSDS CSDS	41.5421899 41.5475275 41.5469167 41.5551604	-81.6707211 -51.6707047 -51.6706619 -81.6701272	444055.0 444055.0 444061.9 444085.0	4599362.8 4599365.3 4599757.9 4599690.0 4598382.5	2195417.1 2195513.2 2195499.2 2195815.1 2195679.7	669722.7 604388.9 606333.7 686111.3 681100.2	11.3 12.1 12.1 12.1	205.6 22.5 29.5 711.7 25.9	2.6 3.5 1.1 1.9	1.9 0.9 0.6	0.7 0.6 0.2	Point Source Linear Contact Point Source (Probable Boulder) Point Source (Probable Boulder) Linear Contact	•
C316 C316 C316 C316	41.5421899 41.5475275 41.5469167 41.5551904 41.5467378	-81.6707211 -81.6707047 -81.6706619 -81.6701272 -81.6701856	444053.0 444053.0 444063.0 444083.0 444083.4	4599062.8 4599065.3 4599757.9 4599699.0 4599699.0	2195417.1 2195513.2 2195459.2 2195515.1 2195679.7 2185644.0	620722.7 604288.9 606333.7 686111.3 681100.2 686047.5	11.3 12.1 12.1 12.1 12.0 11.5	385.6 32.3 25.5 711.7 25.9 485.5	2.6 2.5 1.1 1.9 12.7 2.5	0.9 0.6 0.5 0.4	0.7 0.6 0.2 0.2	Point Source Linear Contact Point Source (Probable Boolder) Point Source (Probable Boolder) Linear Contact Linear Contact	
C316 C316 C316 C316	41.5471899 41.5475275 41.5469167 41.5531804 41.5467378 41.5468811	-81.6707047 -81.6707047 -81.6706619 -81.6701272 -81.6701856 -81.6701475	444055.0 444061.9 444085.0 444085.0 444084.5 444104.5 444102.7	4599045.3 4599045.3 4599757.9 4599890.0 4599889.9 4599039.6	2195417.1 2195513.2 2195513.2 2195490.2 2195515.1 2195679.7 2195644.0 2195674.8	629722.7 604388.9 606333.7 686111.3 681109.2 686047.3 689913.5	11.3 12.1 12.1 12.0 11.5 11.7	385.6 32.3 29.5 711.7 25.9 435.5 184.0	2.6 3.5 1.1 1.9	0.9 0.6 0.5 0.4 0.7	0.7 0.6 0.2	Point Source Linear Contact Point Source (Probable Boalder) Point Source (Probable Boalder) Linear Contact Line	
CSD6 CSD6 CSD6 CSD6 CSD6 CSD6 CSD6	41.5471839 41.5475275 41.5469167 41.5531904 41.5467978 41.5467978 41.5468311 41.5465363	-81.6707211 -81.6707047 -81.6706619 -81.6701272 -81.6701856 -81.6701475 -81.6700519	444051.9 444061.9 444065.0 444089.4 444104.5 444102.7 444113.8	4599062.8 4599065.3 4599757.9 4599699.0 4599699.0	2199417.1 2199313.2 2199499.2 2199819.1 2199879.7 2199674.0 2199674.8 2199688.3	683722.7 604388.9 606333.7 686111.3 681109.2 686047.3 689913.5	113 121 121 121 120 115 117 121	385.6 32.3 25.5 711.7 25.9 485.5	2.6 3.5 1.1 1.9 12.7 2.5 2.7 21.8	0.9 0.6 0.5 0.4 0.7 14.2	0.7 0.6 0.2 0.2 0.7	Point Source Linear Contact Point Source (Probable Boulder) Point Source (Probable Boulder) Linear Contact Linear Contact Linear Contact Linear Contact Linear Contact Linear Contact Linear Contact Linear Contact Linear Contact	
CSD6 CSD6 CSD6 CSD6 CSD6 CSD6 CSD6	41.5471839 41.5475275 41.5469167 41.5531904 41.5467978 41.5467978 41.5468311 41.5465363	-81 6707211 -81 6707047 -81 6706619 -81 6701272 -81 6701856 -81 6701675 -81 6599685	444055.0 444061.9 444085.0 444085.0 444084.5 444104.5 444102.7	459042.3 459045.3 459045.3 4599690.0 4590362.3 4599699.9 4599424.2	2189417.1 2189313.2 2199490.2 2199818.1 2199879.7 2199844.0 2199878.3 2189888.3	629722.7 604388.9 606333.7 686111.3 681109.2 686047.3 689913.5	11.3 12.1 12.1 12.0 11.5 11.7	205.6 22.3 23.5 711.7 25.9 455.5 184.0 71.7 541.4	2.6 3.5 1.1 1.9 12.7 2.5 2.7	0.9 0.6 0.5 0.4 0.7	0.7 0.6 0.2 0.2 0.7	Point Source Linear Contact Point Source (Probable Boalder) Point Source (Probable Boalder) Unier Contact Linear Contact	
C306 C306 C306 C306 C310 C311 C311	41.5471899 41.5475275 41.5469167 41.5531904 41.5467978 41.5467978 41.5465159 41.5465159 41.5389676	-81 6707211 -81 6707047 -81 6706619 -81 6701272 -81 6701856 -81 6701675 -81 6599685	444055.0 444055.0 444061.9 444085.0 444085.0 444108.7 444108.7 444108.7 444108.7	459902.8 459902.3 4599025.3 4599030.0 4599030.0 4599030.0 4599030.6 4599030.6	2199417.1 2199313.2 2199499.2 2199819.1 2199879.7 2199674.0 2199674.8 2199688.3	603722.7 604398.9 606333.7 606111.5 601109.2 609047.5 609913.5 605341.9	11.5 12.1 12.1 12.0 11.5 11.7 12.1 10.6	385.6 32.5 29.5 711.7 25.9 485.5 184.0 71.7	2.6 2.5 1.1 1.9 12.7 2.5 2.7 2.13 2.6	0.9 0.6 0.5 0.4 0.7 14.2	0.7 0.6 0.2 0.2 0.3	Point Source Linear Contact Opint Source (Probable Soulder) Point Source (Probable Soulder) Linear Contact Linear Reflectivity Patch (Poisible Stag)	
CSD6 CSD6 CSD6 CSD6 CSD6 CSD3 CSD3 CSD3 CSD3 CSD3 CSD3 CSD3 CSD3	41.5475275 41.5475275 41.5499107 41.5531004 41.5457578 41.54698911 41.5465263 41.5465263 41.5465263 41.5466878	-81 6707211 -81 6707047 -81 6706619 -81 6701272 -81 6701875 -81 6701875 -81 6700819 -81 669685 -81 6696700 -81 6696700 -81 66967967	049033.1 049050.0 049051.9 049050.0 049089.4 049102.7 049102.7 049102.1 449122.1 449122.7	4596962.8 459965.3 459965.3 4599690.0 4599690.0 459969.9 459969.9 459969.4 4599600.4 4599600.4 459977.0 4599641.8	2195417.1 2195513.2 2195513.2 2195490.2 2195815.1 2195675.7 2195674.8 2195684.0 2195705.6 2195705.6	603722.7 604388.9 605333.7 606111.5 601109.2 606047.5 609313.5 60521.0 605221.0 605027.2	11.5 12.1 12.1 12.0 11.5 11.7 12.1 10.6 12.0 12.0	223 223 235 711.7 25.9 485.5 184.0 74.7 541.4 85.1 32.7 33.1	2.6 2.5 1.1 1.9 12.7 2.5 2.7 21.8 2.6 5.0	1.9 0.9 0.6 0.5 0.4 0.7 14.2 0.3 1.2 0.4 0.7	0.5 0.6 0.2 0.3 0.3 	Point Source Linear Contact Point Source (Probable Boalder) Point Source (Probable Boalder) Linear Contact	
CS 105 CS	41.5471703 41.547974 41.5469197 41.5581904 41.5467978 41.5467978 41.5467163 41.5467163 41.5467163 41.5467163 41.5467163 41.5467163 41.5467163 41.5467163 41.5467163	41 6707211 41 6707647 41 6706619 41 6701275 41 6701475 41 6700475 41 669625 41 6696294 41 6697296 41 6697296 41 6697296	494039.1 49405.0 49405.9 494089.4 494089.4 494102.7 494102.7 494122.1 494122.1 494123.1 494124.5 494124.5	4590962.8 459045.3 459045.3 4599090.0 4590382.3 4599699.9 4590424.2 4599600.4 4590707.1 45996777.A 4599677.A	2195417.1 2195513.2 2195490.2 2195490.2 2195675.7 2195674.0 2195674.3 2195705.0 2195786.2 2195786.2 2195786.2	603722.7 604388.9 606333.7 686111.5 687139.2 686047.5 689313.5 685241.9 665321.0 63389.1 66642.6 662357.2 662357.2	113 121 121 121 120 115 11.7 121 10.6 12.0 12.0 12.1 12.1 12.1	223 223 235 711.7 25.9 485.3 184.0 74.7 541.4 85.1 32.7 33.1 369.0	2.6 2.5 1.1 1.9 12.7 2.5 2.7 21.8 2.6 5.0 10.4 4.5 3.1	1.9 0.5 0.6 0.5 0.4 0.7 14.2 0.8 12.2 0.4 0.7 0.3	0.5 0.6 0.2 0.3 0.3 -	Point Source Linear Contact Point Source (Probable Boalder) Point Source (Probable Boalder) Point Source (Probable Boalder) Linear Contact Linear Li	
C385 C386 C386 C386 C386 C311 C311 C313 C314 C315 C316 C317	41,5421899 41,5475275 41,5469167 41,5551809 41,5467978 41,546798 41,5467	41.6707211 41.6707047 41.6706419 41.6701272 41.6701273 41.670519 41.6606780 41.6606780 41.6606780 41.6606790 41.6606790 41.6606790 41.6606790	484033.1 48405.0 48405.9 484065.9 484085.9 484085.9 484102.7 484102.7 484122.1 484123.1 484123.9 484123.9	459092.3 4590925.3 4590925.3 4599890.0 4599923.5 459969.9 459969.3 4599600.6 459600.6 4596777.1 4596977.6 4596977.6 4596977.6	2109417.1 2190513.2 2190513.1 2190409.2 2190619.7 2190674.8 2190674.8 2190705.6 2190705.8 2190705.3 2190705.3 2190705.3	603722.7 604388.9 606333.7 686110.5 681109.2 686047.3 682109.2 685021.0 605421.0 605421.0 605421.0 605421.0 605421.0	113 121 121 120 115 117 120 120 120 120 121 121 105	285.6 22.3 22.5 711.7 25.9 425.5 184.0 71.7 541.4 85.1 22.7 33.1 565.0 528.1	2.6 3.5 1.1 1.9 12.7 2.5 2.7 2.13 2.6 5.0 10.4 4.5 3.1	1.9 0.9 0.6 0.5 0.4 0.7 14.2 0.3 1.2 0.4 0.7 0.3 14.8	0.5 0.6 0.2 0.3 0.3 	Point Source Linear Centacs Point Source (Probable Bos Iden) Point Source (Probable Bos Iden) Point Source (Probable Bos Iden) Linear Centacs	•
GH G	41.5421898 41.5498147 41.5498147 41.5581904 41.5581904 41.558193 41.568113 41.568113 41.568113 41.568113 41.568113 41.568113 41.568113 41.568113 41.568113 41.568113 41.568113 41.568113 41.568113 41.568113	41.6707211 41.6707047 41.670617 41.6701272 41.6701272 41.6701275 41.6606194 41.6606194 41.6606194 41.6606194 41.6606194 41.6606194 41.6606194 41.6606194 41.6606194 41.6606194	040023.1 040055.0 04005.0 04005.0 040089.4 04000.7 040103.7 040103.7 040103.4 040103.4 040103.4 040103.4 040103.4 040103.6 040103.6 040103.6 040103.6 040103.6	4596942.3 459615.3 459615.7.2 4595690.0 4599690.3 4599690.3 4599690.3 4599690.3 4599600.3 459060.3 459077.3 459077.3 459077.3 459077.3 459077.3 459077.3	2195417.1 2195513.2 2195490.2 2195490.2 2195675.7 2195674.0 2195674.3 2195705.0 2195786.2 2195786.2 2195786.2	603722.7 604388.9 606333.7 686111.5 687139.2 686047.5 689313.5 685241.9 665321.0 63389.1 66642.6 662357.2 662357.2	113 121 121 121 120 115 11.7 121 10.6 12.0 12.0 12.1 12.1 12.1	223 223 235 711.7 25.9 485.3 184.0 74.7 541.4 85.1 32.7 33.1 369.0	2.6 2.5 1.1 1.9 12.7 2.5 2.7 21.8 2.6 5.0 10.4 4.5 3.1	1.9 0.5 0.6 0.5 0.4 0.7 14.2 0.8 12.2 0.4 0.7 0.3	0.5 0.6 0.2 0.3 0.3 	Point Source Linear Contact Point Source (Probable Boalder) Point Source (Probable Boalder) Point Source (Probable Boalder) Linear Contact Linear Li	
GH G	41.5421898 41.5479275 41.5499197 41.5531904 41.5531904 41.5467978 41.5467978 41.546715 41.546715 41.546715 41.546778 41.546778 41.546778 41.546778 41.546778 41.546778 41.5598999 41.5386999 41.5386999 41.5386999	41.6707211 41.6707047 41.6706419 41.6701272 41.6701272 41.6701273 41.6701475 41.6690425 41.6690720 41.6690720 41.6690720 41.6690720 41.6690720 41.6690720 41.6690720	044033.1 04405.0 04405.0 04405.0 044089.4 044102.7 044102.7 044122.1 044122.3 044122.3 044123.8 044148.8 044148.8 044148.8	4590042.3 4590105.3 4590105.3 4590107.7.3 4599089.0 4599069.9 4599069.4 4599029.4 4599007.1 4590077.0 4590041.8 459007.3 4590077.0 459077.0 459077.0 459077.0	2109417.1 2109313.2 210940.2 210940.2 2109413.1 2109414.0 21096414.8 21095614.8 2109751.4 2109751.4 2109751.4 2109761.9 2109761.9 2109761.9 2109761.9	660 722.7 664 188 9 665 333.7 686 181.5 681 18.5 682 18.5 682 18.5 682 18.5 683 28.9 682 49.8 682 49.8 682 49.8 682 49.8 682 49.8 682 49.8 682 49.8	113 121 121 121 120 115 117 121 120 120 120 121 121 108 108 108 109 109 115	205.6 22.3 22.5 711.7 25.9 485.3 184.0 71.F 541.4 85.1 32.7 33.1 35.9 558.1 854.7 552.9 414.2	2.6 2.5 1.1 1.9 12.7 2.5 2.7 21.8 2.6 5.0 10.4 4.5 3.1 33.1 5.0 0.7 10.8	1.9 0.9 0.6 0.5 0.4 0.7 14.2 0.8 1.2 0.4 0.7 0.3 14.8 1.8 0.6 2.1	0.7 0.6 0.2 0.3 0.7 - - 0.2 0.1 0.1	Point Source Linear Contact Probable Bos Iden) Point Source (Probable Bos Iden) Point Source (Probable Bos Iden) Linear Contact Linear Contac	
GB G	41.5421898 42.5475275 42.5469197 43.5551904 41.5467978 41.5467978 41.5467978 41.5469798 41.5469798 41.5469798 41.5469798 41.5589998 41.5589998 41.5589998 41.5599998 41.5599998	41.6707211 41.6707047 41.670617 41.6701272 41.6701272 41.6701275 41.6606194 41.6606194 41.6606194 41.6606194 41.6606194 41.6606194 41.6606194 41.6606194 41.6606194 41.6606194	044033.1 04405.0 04405.0 04405.0 044089.4 044102.7 044102.7 044122.1 044122.3 044122.3 044123.8 044148.8 044148.8 044148.8	4596942.3 459615.3 459615.7.2 4595690.0 4599690.3 4599690.3 4599690.3 4599690.3 4599600.3 459060.3 459077.3 459077.3 459077.3 459077.3 459077.3 459077.3	2109417.1 2109313.2 2109409.2 2109409.2 2109079.7 21096474.8 2109706.8 2109706.8 2109706.3 2109703.3 2109703.3 2109703.3 2109703.3	603722.7 604388.9 606333.7 606111.3 60111.3 601047.3 602047.3 602047.3 602047.3 602047.3 602047.3 602047.3 602047.3 602047.3 602047.3 602047.3 602047.3	113 121 121 121 120 115 117 121 106 120 121 121 105 108	245.6 22.3 22.5 711.7 23.9 445.9 164.0 71.7 541.4 65.1 22.7 33.1 360.0 528.1 854.7 552.9	2.6 2.5 1.1 1.9 12.7 2.8 2.7 21.8 2.6 5.0 10.4 4.5 3.1 33.1 5.0 0.7	1.9 0.9 0.6 0.5 0.4 0.7 14.2 0.8 3.2 0.4 0.7 0.8 14.8 1.8 0.6	0.7 0.6 0.2 0.3 0.7 - - 0.2 0.1	Point Source Linear Contact Point Source (Probable Boalder) Point Source (Probable Boalder) Point Source (Probable Boalder) Linear Contact C	•
GH G	41.5421899 41.5478275 41.5469187 41.5531808 41.5469378 41.54693813 41.5469383 41.546938437 41.556936 41.556936 41.556936 41.556936 41.556936 41.556936 41.556936 41.556936 41.556936	41.6707211 41.6707047 41.6706419 41.6701272 41.6701272 41.6701273 41.600129 41.6606740 41.6606740 41.6606740 41.6606740 41.6606740 41.6606740 41.6606740 41.6606740 41.6606740 41.6606740 41.6606740 41.6606740 41.6606740	044023.1 04405.0 044065.0 044065.0 044085.4 044004.5 044102.7 044102.7 044122.7 044123.0 044124.9 044124.9 044125.0 044125.0 044125.0 044125.0 044125.0 044125.0 044125.0 044125.0 044125.0 044125.0 044125.0 044125.0 044125.0	4596042.3 4596165.3 4596165.3 4596960.2 4599690.2 4599693.3 4599693.4 459673.4 459673.4 459673.3 459673.3 459673.3 459673.3 459673.3 459673.3 459673.3 459673.3 459673.3 459673.3 459673.3	2109417.1 2109313.2 2109409.2 2109419.1 2109479.2 2109414.9 210944.9 210946.3 210976.6 210976.6 210976.6 210976.2 210975.3 210976.2 210976.2 210976.2 210976.3 210976.3 210976.3 210976.3 210976.3	603722.7 6043889 9 605333.7 605111.5 605110.5 605047.5 605047.5 605047.5 605047.5 605047.5 605047.5 605047.5 605047.5 605047.5 605047.5 605047.5 605047.5 605047.5 605047.5 605047.5 605047.5 605047.5 605047.5 605047.5	113 121 121 121 120 115 117 121 122 122 123 124 120 125 126 127 128 128 128 128 128 129 121 121 121 121 121 121 121 121 121	205.6 22.3 22.5 711.7 25.9 485.5 184.0 71.7 541.4 85.1 32.7 33.1 360.0 554.7 552.9 415.4 473.0 17.0	2.6 2.5 1.1 1.9 12.7 2.5 2.7 21.8 2.6 3.0 10.4 4.5 3.1 33.1 33.1 30.0 0.7 10.8 2.8 2.8 2.8	1.9 0.9 0.6 0.5 0.4 0.7 14.2 0.8 1.2 0.4 0.7 0.3 14.8 1.8 0.6 2.1 0.6 2.1 0.8	0.7 0.6 0.2 0.7 0.7 - - 0.2 0.1 0.1 - 0.2	Point Source Linear Contact Probable Boalderi Point Source (Probable Boalderi) Point Source (Probable Boalderi) Linear Contact	
GH G	41.5421899 41.5479273 41.5469167 41.5467978 41.5467978 41.5467978 41.546963 41.546963 41.546976 41.546976 41.546976 41.546976 41.546976 41.554697 41.554697 41.554697 41.5546989 41.5546989 41.5546989 41.5546989 41.5546989 41.5546989 41.5546989 41.5546989 41.5546989 41.5546989 41.5546989 41.5546989 41.5546989	41.6707211 41.6707047 41.670547 41.6701272 41.6701272 41.6701275 41.6701275 41.690625 41.690720 41.690720 41.690720 41.690720 41.690720 41.690720 41.690720 41.690720 41.690720 41.690720 41.690720 41.690720 41.690720	044023.1 044005.0 044005.0 044005.0 044005.0 044002.7 044102.7 044123.1 044123.1 044123.1 044123.0 044125.5 044125.0 044125.0	459604.3 459015.3 459015.3 459090.7 4599800.1 459015.3 459605.4 459605.4 459605.4 459605.4 459605.3 459605.3 459605.3 459605.3 459605.3 459605.3 459655.3 459656.3 45966	2109417.1 2199313.2 2199490.2 2199490.2 2199813.1 2199679.7 219964.0 219968.0 2199750.3 2199750.3 2199750.3 2199750.3 2199750.3 2199750.3 2199750.3 2199750.3 2199750.3 2199750.3 2199750.3	603722.7 604388.9 606333.7 686110.5 687109.2 685047.3 685047.3 68521.0 605421.0 605421.0 605421.0 605421.0 605421.0 605421.0 605421.0 605421.0 605421.0 605421.0 605421.0 605421.0 605421.0 605421.0 605421.0 605421.0 605421.0	113 121 121 121 120 115 117 121 106 120 121 121 103 106 100 105 115 115 115 115 116	205.6 22.3 22.5 711.7 23.9 485.3 194.0 71.7 541.4 85.1 22.7 33.1 569.0 528.1 654.7 532.9 414.2 417.0	2.6 2.5 1.1 1.9 12.7 2.5 2.7 2.18 2.6 5.0 10.4 4.5 3.1 33.1 33.1 33.1 3.0 0.7 10.8 2.8 2.9	1.9 0.9 0.6 0.5 0.4 0.7 14.2 0.7 0.8 14.8 1.8 0.6 2.1 0.5 0.6	0.7 0.6 0.2 0.7 0.7 	Point Source Linear Contact Probable Bos Iden) Point Source (Probable Bos Iden) Point Source (Probable Bos Iden) Linear Contact Linear Contac	M71 M39
GH G	41,5421899 41,5469167	41.6707211 41.6707047 41.6706419 41.6701896 41.6701896 41.6701896 41.600700 41.600700 41.600730 41.600730 41.600730 41.600730 41.600730 41.600730 41.600730 41.600730 41.600730 41.600730 41.600730 41.600832 41.600832 41.600832 41.600832 41.600832 41.600832 41.600832 41.600832 41.600832 41.600832 41.600832 41.600832 41.600832 41.600832 41.600832 41.600832 41.600832 41.600832	040023.1 04005.0 044005.0 044005.0 044009.5 044102.7 044102.7 044122.7 444125.1 044108.8 044104.9 044105.9 044105.0 044105.0 044105.0 044105.0 044105.0 044105.0 044105.0 044105.0 044105.0 044105.0 044105.7	4596943.3 4596957.3 4596950.0 4599690.0 4599690.3 4599690.3 4599690.3 4599690.3 4599690.3 4599690.3 4599697.3 4599677.3 4599677.3 4599677.3 4599677.3 4599677.3 4599677.3 4599677.3 4599677.3 4599677.3 4599677.3 4599677.3 4599677.3 4599677.3 4599677.3 4599677.3 4599677.3 4599677.3 4599677.3	2109417.1 2109313.2 2109490.3 2109490.3 2109679.7 2109674.8 2109750.3 210975	603722.7 604388.9 606333.7 680181.3 68108.3 682047.5	113 121 121 121 121 120 115 117 121 106 120 121 121 103 106 100 105 115 115 115 116 106 107 108 117 108 108 108 108 108 108 108 108 108 108	205.6 22.3 22.5 711.7 23.9 445.9 164.0 71.7 541.4 65.1 22.7 33.1 360.0 528.1 854.7 444.2 473.0 473.0 674.3	2.6 2.5 1.1 1.9 12.7 2.8 2.7 21.8 2.6 5.0 10.4 4.5 3.1 33.1 33.1 30.0 0.7 10.8 2.8 2.9 4.9 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0	1.9 0.9 0.6 0.5 0.4 0.7 34.2 0.3 3.2 0.4 0.7 0.3 34.8 1.8 0.6 2.1 0.5 0.8	0.7 0.6 0.2 0.7 0.7 	Point Source Linear Contact Point Source (Probable Bos Iden) Point Source (Probable Bos Iden) Point Source (Probable Bos Iden) Linear Contact	M71 M39
CHE	41.5421899 41.542925 41.5469167 41.5531900 41.5469313 41.5469313 41.5461190 41.5561190 4	41.6707211 41.6707047 41.670643 41.6703272 41.6703273 41.670354 41.670354 41.660730 41.6607	044023.1 04405.0 044001.9 044005.0 044005.0 0440089.4 044103.7 044113.8 044123.1 044123.1 044125.1 044125.9 044136.6 044145.9 044136.7 044136.7 044136.7 044136.7 044136.7 044136.7 044136.7 044136.7 044136.7 044136.7	4596762.3 4596757.3 4599690.2 4599690.2 4599690.3 4599690.3 4599690.3 4599690.3 459670.3 459670.3 459670.2 459670.2 459670.2 459670.2 459670.2 459670.2 459670.2 459670.2 459670.2 459670.3 459670.2 459670.3 4596	2109417.1 2109313.2 2109409.2 2109419.1 2109614.8 2109614.8 21096614.8 210976.6 210976.6 210976.6 210976.1 2109770.3	603 722.7 604 3281 9 605 333.7 605 111.5 601 113.5 605 121.5 605 121.5 605 121.6 605 121.6	113 121 121 121 120 115 117 121 126 120 121 121 108 108 108 115 115 115 115 115 115 115 115 115 11	205.6 22.3 22.5 711.7 25.9 184.0 74.7 541.4 85.1 32.7 33.1 350.0 528.1 544.7 552.9 414.2 415.4 472.0 17.0 544.3 130.6 64.3 130.6 64.3 130.6 64.3 130.6 64.3 130.6 64.3 130.6 64.3 130.6 64.3 130.6 64.3 130.6 64.3 130.6 64.3 130.6 64.3 130.6 64.3 130.6 64.3 130.6 130	2.6 2.5 1.1 1.9 12.7 2.5 2.6 2.6 5.0 10.4 4.5 3.1 33.1 33.1 2.8 2.8 2.9 4.0 11.9	19 0.9 0.6 0.5 0.4 0.7 14.2 0.3 1.2 0.4 0.7 0.3 14.8 1.8 0.6 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5	0.7 0.6 0.2 0.2 0.7 - - 0.2 0.1 0.1 - - 0.2 0.1 0.1 - - 0.3 0.3 0.1 0.1 - 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	Point Source Linear Contact Probable Bos Iden) Point Source (Probable Bos Iden) Point Source (Probable Bos Iden) Linear Contact Linear Contac	M71 M139
G18 G19 G11 G11 G11 G13 G13 G13 G13 G13 G13 G13	41.5421899 41.5479273 41.5469167 41.5467978 41.5467978 41.5468563 41.5468563 41.5468563 41.5468563 41.5468563 41.5468563 41.5468797 41.5468879 41.5468877 41.546	41.6707211 41.6707047 41.6706419 41.6701896 41.6701896 41.6701896 41.6701896 41.6809685 41.6809780 41.680	040023.1 04005.0 044005.0 044005.0 044005.0 044008.4 044108.7 044108.7 044128.7 044128.7 044128.8 044108.8	459604.3 4590165.3 4590165.3 4599690.0 4599690.0 4599699.0 4599699.0 4599699.0 4599600.0	2109417.1 2109313.2 2109403.2 2109403.2 2109403.2 2109413.1 2109473.2 2109474.0 2109474.3 2109475.3 2109575.3 2109575.3 2109575.4 2109575.4 2109575.4 2109575.3	669 722.7 664 381 9 665 333.7 681 111.3 681 110.2 682 687 13.5 682 787 3.6 683 787	113 121 121 121 120 115 117 121 108 108 120 121 121 108 108 118 118 118 118 118 118 118 11	245.6 22.2 22.5 27.1.7 25.9 485.3 184.0 71.7 541.4 85.1 32.7 33.1 35.1 35.1 35.1 35.1 35.1 35.1 35.1	2.6 2.5 1.1 1.9 12.7 2.3 2.5 2.7 2.13 2.6 5.0 10.4 4.5 3.1 3.0 0.7 10.8 4.5 10.7 10.8 4.5 10.7 10.8 10.7 10.8 10.8 10.8 10.8 10.8 10.8 10.8 10.8	1.9 0.9 0.6 0.5 0.4 0.7 14.2 0.3 12.2 0.4 0.7 0.5 14.8 14.8 1.8 0.6 0.7 0.8 0.2 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8	0.7 0.6 0.2 0.2 0.7 - - 0.2 0.1 0.1 - - 0.2 0.1 0.1 - - 0.3 0.3 0.1 0.1 - 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	Point Source Linear Contact Probable Bos bleri Point Source (Probable Bos bleri Point Source (Probable Bos bleri Point Source (Probable Bos bleri Linear Contact Linear Con	M71 M139
CHE	41.5491898 41.549187 41.549187 41.549187 41.549583 41.549583 41.549583 41.549583 41.549583 41.549583 41.549687 41.559939 41.559887	41 6707211 41 670747 41 670643 41 670277 41 670549 41 670549 41 670549 41 669645 41 669739 41 669739	040023.1 04005.0 044005.0 044005.0 044005.0 044008.4 044002.7 044103.0 044123.0 044123.0 044123.0 044123.0 044127.0 044177.0 044177.0 044177.0 044179.1	4590042.3 4590165.3 4590165.3 4590165.3 4599689.0 4599689.9 4599689.3 4599689.3 4599689.3 459007.1 459077.6	2109417.1 2109313.2 2109400.3 2109400.3 2109400.3 2109400.3 2109400.3 2109400.3 2109400.3 2109500.3 2109500.3 2109500.3 2109500.3 2109500.3 2109500.3 2109600.3 2109600.3 2109600.3 2109600.3 2109600.3	600 722.7 604 320 9 605 333.7 605 111.5 605 111.5 605 125.5 605 241.9 605 241.9 605 242.0 605 247.5 605 247.6 605 247.6	113 121 121 121 120 115 117 121 106 120 121 103 106 100 105 115 115 115 115 115 115 115 115	205.6 22.2 22.5 711.7 25.9 485.5 184.0 71.F 541.6 85.1 22.T 33.1 35.2 455.9 414.2 415.4 415.4 415.6 417.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0	2.6 2.5 1.1 1.9 12.7 2.5 2.7 2.13 2.6 3.0 3.1 3.1 3.1 3.1 3.1 3.1 3.1 3.1 3.1 3.1	1.9 0.9 0.6 0.5 0.4 0.7 14.2 0.3 12.2 0.4 0.7 0.5 14.8 14.8 1.8 0.6 0.6 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	0.3 0.8 0.2 0.3 0.7 	Point Source Linear Centact Point Source (Probable Bos Iden) Point Source (Probable Bos Iden) Point Source (Probable Bos Iden) Linear Centact	M71 M29
GB G	41.5491899 41.549197 41.5591904 41.549197 41.5591904 41.549197 41.549191 41.549593 41.549697 41.549697 41.549697 41.549697 41.549697 41.549697 41.549697 41.549697 41.549697 41.549799 41.5597999 41.5597999 41.5597999 41.5597999 41.5597999 41.5597999 41.5597999 41.5597999 41.5597999 41.549799 41.549799 41.549799 41.549799 41.549799 41.549799 41.549799 41.549799 41.549799 41.549799 41.549799 41.549799 41.549799 41.549799 41.549799 41.549799 41.549799 41.549799 41.549799	41 6707211 41 670747 41 670643 41 6701277 41 6701475 41 6700549 41 660032 41 6600	040023.1 04005.0 044005.0 044005.0 044005.0 044005.0 044005.0 044005.0 044103.0 044123.1 044123.1 044123.1 044123.0 044136.0	4590042.3 4590105.3 4590107.3 4599109.0 4599109.0 4599109.0 4599009.4 459000.4 459000.4 459000.4 459000.4 459000.4 459000.3 4590000.3 459000.3 459000.3 459000.3 459000.3 459000.3 459000.3 4590	2109417.1 2109313.2 2109400.3 2109400.3 2109400.3 2109607.3 2109607.3 2109607.3 2109705.6	603 722.7 604 3281 9 605 333.7 605 111.5 605 110.5 605 120.5 605 241.0 605 242.0 605 242.0 605 245.1 605 245.2 605 245.2	113 121 121 121 121 120 115 117 121 122 122 121 123 108 100 105 115 115 115 115 115 115 115 115	205.6 22.3 22.5 27.1.7 25.9 485.5 184.0 74.7 541.6 85.1 22.7 33.1 550.6 494.7 552.9 414.2 415.4 475.4 475.0 52.0 52.0 52.0 52.0 52.0 52.0 52.0 5	2.6 2.5 1.1 1.9 12.7 2.5 2.7 2.13 2.6 5.0 10.4 4.5 3.1 3.0 0.7 2.8 2.9 2.9 2.9 1.0 3.1 1.0 3.1 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1	1.9 0.9 0.6 0.5 0.4 0.7 0.3 14.2 0.4 0.7 0.5 14.8 0.6 2.3 0.5 0.6 0.5 0.6 0.5 0.6 0.7 0.6 0.5 0.6 0.5 0.6 0.5 0.6 0.5 0.6 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5	0.7 0.6 0.2 0.2 0.7 0.7 0.2 0.1 0.1 0.2 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	Point Source Linear Contact Probable Bos Iden) Point Source (Probable Bos Iden) Point Source (Probable Bos Iden) Linear Contact Linear Contac	M71 M139
GB G	41.5491898 41.549187 41.549187 41.549187 41.549181 41.549587 41.549587 41.549678 41.549678 41.549678 41.549678 41.549678 41.549678 41.549678 41.549678 41.549678 41.549789 41.549789 41.549789 41.549789 41.549789 41.549789 41.549789 41.549789 41.549789	41 6707211 41 670747 41 670643 41 6701272 41 6700549 41 6700549 41 6600635 41 6600749 41 6600749 41 660749 41 6	040023.1 044055.0 044005.0 044005.0 044005.0 044005.0 044004.5 044104.5 044123.1 044123.1 044123.5 044125.0	4590042.3 4590105.3 4590105.3 4590107.3 4599109.0 4599109.3 4599109.3 4599109.3 4599109.3 459010	2109417.1 2109313.2 2109409.2 2109409.2 2109413.1 2109479.3 210944.0 210944.0 210944.0 210944.0 210945.2 210975.2 210975.4 2109775.3 210975.4 2109775.3 210946.4 210946.4 210946.4 210968.6	603 722.7 604 388 9 605 333.7 605 111.5 605 110.5 605 110.5 605 121.5 605 121.5	113 121 121 121 121 121 120 115 117 121 120 121 121 120 121 121 120 130 145 115 110 120 121 121 121 121 121 121 121 121	205.6 22.3 22.5 711.7 25.9 485.5 184.0 74.7 541.4 85.1 32.7 33.1 360.0 552.6 415.4 470.0 541.4 21.0 552.6 125.0 552.6 125.0 125.0 125.0 125.0 125.0 125.0 125.0 125.0 125.0 125.0 125.0 125.0 125.0 125.0 125.0 125.0 125.0	2.6 2.5 1.1 1.9 12.7 2.5 2.7 2.13 2.6 5.0 0.7 2.9 2.9 2.9 2.9 11.9 2.9 11.9 11.7 7.8 3.3 1.1 7.8 3.3 1.1 7.8 3.3 1.1 7.8 1.1 7.8 7.8 7.8 7.8 7.8 7.8 7.8 7.8 7.8 7.8	1.9 0.6 0.5 0.4 0.7 14.2 0.3 12.0 0.3 14.8 14.8 14.8 1.8 0.6 0.6 0.8 0.7 0.7 0.8 0.7 0.7 0.8 0.7 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8	0.7 0.6 0.2 0.2 0.7 0.7 0.2 0.1 0.1 0.2 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	Point Source Linear Contact Point Source (Probable Bos bler) Point Source (Probable Bos bler) Point Source (Probable Bos bler) Linear Contact	M73
G18 G18 G18 G19 G11 G11 G11 G11 G11 G11 G11 G11 G11	41.5491899 41.549197 41.5591904 41.549197 41.5591904 41.549593 41.549593 41.549593 41.549593 41.549593 41.549593 41.549593 41.549593 41.549593 41.549593 41.549593 41.549793 41.549793 41.549793 41.549793 41.549793 41.549793 41.549793 41.549793 41.549793 41.549793 41.549793 41.549793 41.549793 41.549793 41.549793 41.549793 41.549793	41 6707211 41 670747 41 670643 41 6701277 41 6700549 41 6700549 41 660065 41 660767 41 6607	040023.1 04005.0 044005.0 044005.0 044005.0 044005.0 044005.0 044005.0 044103.0 044103.0 044123.1 044123.1 044123.1 044123.0	4590042.3 4590165.3 4590165.3 4590177.3 45991890.3 45991890.3 45991890.3 4599189.3 4590189.4 4590189.4 4590189.3 459	2109417.1 2109313.2 2109400.3 2109400.3 2109400.3 2109400.3 2109601.8 2109601.8 2109601.8 210970	603 722.7 604 3281 9 605 333.7 605 111.5 605 110.5 605 120.5 605 241.9 605 241.9 605 242.0 605 247.2 605 247.2	113 121 121 121 121 120 115 117 121 102 122 121 121 103 106 100 105 115 115 115 115 115 115 115 115	205.6 22.3 22.5 27.11.7 25.9 485.5 184.0 71.7 541.4 85.1 22.7 33.1 569.0 552.9 414.2 415.4 417.0 57.0 57.0 57.0 57.0 57.0 57.0 57.0 5	2.6 2.5 1.1 1.9 12.7 2.5 2.7 2.13 2.6 5.D 10.4 4.5 3.1 3.1 3.1 10.8 2.8 2.8 2.9 11.9 11.7 7.6 11.7 11.7 11.7 11.7 11.7 11.7	1.9 0.9 0.6 0.5 0.4 0.7 14.2 0.3 3.2 0.4 0.7 0.5 14.8 1.8 1.8 2.1 0.5 2.1 0.5 0.8 0.8 0.7 1.2 0.9 0.8 0.9 0.9 0.8 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9	0.7 0.6 0.2 0.3 0.7 0.2 0.1 0.1 0.2 0.3 0.3 0.1 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	Point Source Linear Contact Probable Boalderi Point Source (Probable Boalderi) Point Source (Probable Boalderi) Point Source (Probable Boalderi) Linear Contact Linear Cont	M71 M29
GB G	41.5491898 41.549187 41.549187 41.549187 41.549181 41.549583 41.549583 41.5496833 41.549	41 6707211 41 670747 41 670643 41 6701272 41 6701273 41 6700549 41 6700549 41 6600635 41 6600720 41 66007	040023.1 04005.0 044005.0 044005.0 044005.0 044005.0 044005.0 044103.5 044123.1 044123.1 044123.1 044123.1 044125.7 044125.7 044125.7 044125.7 044125.7 044125.7 044125.7 044125.7 044125.7 044125.7 044125.7 044125.7 044125.7 044125.7 044125.7 044125.7 044125.7 044125.7 044125.7	4590042.3 4590105.3 4590107.3 4599190.0 4599182.3 4599690.3 4599600.4 459000.4 459000.4 459000.4 459000.4 459000.3 4590000.3 459000.3 459000.3 459000.3 459000.3 459000.3 459000.3 4590	2109417.1 2109313.2 2109409.2 2109409.2 2109409.2 2109409.3 2109409.3 2109409.3 2109409.3 2109409.3 2109709.3	603 722.7 604 388 9 605 333.7 605 111.5 605 110.5 605 110.5 605 121.5 605 121.5	113 121 121 121 121 120 115 117 121 120 121 121 103 106 105 115 115 110 120 121 121 121 121 121 121 121 121	245.6 22.3 22.5 711.7 25.9 485.5 184.0 74.7 541.4 85.1 22.7 33.1 550.6 454.7 542.9 415.4 473.0 506.0 17.0 644.3 113.0 506.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12	2.6 2.5 1.1 1.9 12.7 2.5 2.7 2.13 2.6 2.7 2.13 2.6 4.5 3.1 1.04 4.5 3.1 1.00 3.5 1.00 4.5 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.	1.9 0.6 0.6 0.5 0.4 0.7 14.2 0.3 12.2 0.4 0.7 0.5 14.8 14.8 1.8 0.6 0.6 0.8 0.7 1.2 0.5 0.9 0.7 1.2 1.2 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5	0.7 0.6 0.2 0.2 0.7 0.7 0.2 0.1 0.1 0.2 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	Point Source Linear Contact Probable Bos Iden) Point Source (Probable Bos Iden) Point Source (Probable Bos Iden) Point Source (Probable Bos Iden) Linear Contact Linear Con	M73
CHE	41.5479275 41.5469167 41.5531904 41.5469167 41.5531904 41.5469811 41.5469811 41.5469813 41.5469813 41.5469813 41.5469813 41.5469813 41.5469813 41.5469813 41.5469813 41.5469813 41.5469813 41.5469813 41.5469813 41.546983 41.546983 41.546983 41.546983 41.546983 41.546983 41.546983 41.546983 41.546983 41.546983 41.546983 41.546983 41.546983 41.546983	41 6707211 41 6707047 41 6706419 41 6700479 41 6700479 41 6700519 41 6700519 41 6809329 41 6809720 41 680	044023.1 044035.0 044001.9 044005.0 044005.0 0440089.4 044102.7 044113.8 044123.1 044123.1 044125.1 044125.0	459604.3 459645.3 459645.3 459690.0 459960.0 4599	2109417.1 2109313.2 2109409.2 2109409.2 2109419.7 21096719.7 21096714.8 21096714.8 2109709.6	603 722.7 604 388 9 605 333.7 605 131.5 605 131.5 605 131.5 605 131.5 605 131.9 605 221.0 605 221.0 605 221.0 605 237.2 605 244.2 605 247.5 607 244.1 607 247.7 607 247.7	113 121 121 121 121 121 120 115 117 121 126 120 121 105 106 105 115 115 110 98 120 1115 1119 120 1119 119 114 1111	205.6 22.3 22.5 22.5 22.5 22.5 22.7 22.9 22.9 2485.5 184.0 74.7 541.4 85.1 22.7 23.1 260.0 528.1 260.0 528.1 270.0 544.5 270.0 544.5 270.0 544.5 270.0 544.5 270.0 544.5 270.0 544.5 270.0 544.5 270.0 544.5 270.0	2.6 2.5 1.1 1.9 12.7 2.5 2.7 2.13 2.6 5.D 0.7 10.04 4.5 3.1 10.7 10.8 2.8 2.9 10.9 10.9 10.9 10.9 10.9 10.9 10.9 10	1.9 0.9 0.6 0.5 0.4 0.7 14.2 0.3 1.2 0.4 0.7 0.3 1.2 0.4 0.7 0.3 1.2 0.6 0.5 0.6 0.7 0.8 0.7 0.9 0.8 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9	0.7 0.6 0.2 0.3 0.3 0.3 0.1 0.1 0.2 0.8 0.8 0.3 0.1 0.7 0.7	Point Source Linear Contact Point Source (Probable Bos Iden) Point Source (Probable Bos Iden) Point Source (Probable Bos Iden) Linear Contact	M73
GB G	41.5471890 41.5479275 41.549167 41.5531904 41.549581 41.549583 41.549583 41.549583 41.549583 41.549635 41.549635 41.549635 41.549635 41.549635 41.549635 41.549635 41.54963 41	41 6707211 41 670747 41 670643 41 6701277 41 6701475 41 6700549 41 6609485 41 6609485 41 6609747 41 66097	040023.1 04005.0 044005.0 044005.0 044005.0 044005.0 044005.0 044103.5 044123.1 044123.1 044123.1 044123.1 044125.7 044125.7 044125.7 044125.7 044125.7 044125.7 044125.7 044125.7 044125.7 044125.7 044125.7 044125.7 044125.7 044125.7 044125.7 044125.7 044125.7 044125.7 044125.7	4590042.3 4590105.3 4590107.3 4599190.0 4599182.3 4599690.3 4599600.4 459000.4 459000.4 459000.4 459000.4 459000.3 4590000.3 459000.3 459000.3 459000.3 459000.3 459000.3 459000.3 4590	2109417.1 2109313.2 2109409.2 2109409.2 2109409.2 2109409.3 2109409.3 2109409.3 2109409.3 2109409.3 2109709.3	603 722.7 604 388 9 605 333.7 605 111.5 605 110.5 605 110.5 605 121.5 605 121.5	113 121 121 121 121 120 115 117 121 120 121 121 103 106 105 115 115 110 120 121 121 121 121 121 121 121 121	245.6 22.3 22.5 711.7 25.9 485.5 184.0 74.7 541.4 85.1 22.7 33.1 550.6 454.7 542.9 415.4 473.0 506.0 17.0 644.3 113.0 506.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12	2.6 2.5 1.1 1.9 12.7 2.5 2.7 2.13 2.6 2.7 2.13 2.6 4.5 3.1 1.04 4.5 3.1 1.00 3.5 1.00 4.5 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.	1.9 0.6 0.6 0.5 0.4 0.7 14.2 0.3 12.2 0.4 0.7 0.5 14.8 14.8 1.8 0.6 0.6 0.8 0.7 1.2 0.5 0.9 0.7 1.2 1.2 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5	0.7 0.6 0.2 0.3 0.7 0.2 0.1 0.1 0.2 0.3 0.3 0.1 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	Point Source Linear Contact Probable Bos Iden) Point Source (Probable Bos Iden) Point Source (Probable Bos Iden) Point Source (Probable Bos Iden) Linear Contact Linear Con	M73
G18 G18 G19 G19 G11 G11 G11 G11 G11 G11 G11 G11	41.547289 41.547275 41.549167 41.5531904 41.549563 41.549633 41.549633 41.549633 41.549633 41.549633 41.549633 41.549633 41.549633 41.549633 41.549633 41.549633 41.549633 41.549633 41.549633 41.549633 41.549633	41 6707211 41 6707047 41 6706419 51 6701475 41 6700519 41 6700519 41 680730 41 68	044023.1 04405.0 044095.0 044095.0 044099.4 044103.7 044113.8 044123.1 044125.1 044125.0	4590042.3 4590105.3 4590105.3 4590107.3 4599109.0 4599109.3 4599009.3 4599009.4 4590007.1 459007.7 459007.3	2109417.1 2109313.2 2109409.2 2109409.2 2109414.0 2109674.8 2109674.8 2109709.6	603 722.7 604 3281 9 606 333.7 606 131.5 607 131.5	113 121 121 121 121 121 120 115 117 121 126 120 121 121 105 106 105 115 110 107 111 111 111 111 111 111 111 111	205.6 22.3 22.5 22.5 22.5 22.5 22.5 22.7 22.7 22.9 24.5 26.7 26.7 26.7 26.7 26.7 26.7 26.7 26.7	2.6 2.5 1.1 1.9 12.7 2.5 2.7 2.13 2.6 5.D 0.7 10.04 4.5 3.1 10.07	1.9 0.9 0.6 0.5 0.4 0.7 14.2 0.8 1.2 0.4 0.7 0.8 1.8 0.6 2.3 1.9 0.6 0.7 0.8 0.8 0.9 0.8 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9	0.7 0.6 0.2 0.3 0.3 0.3 0.1 0.1 0.2 0.8 0.8 0.3 0.1 0.7 0.7	Point Source Linear Contact Point Source (Probable Bos bler) Point Source (Probable Bos bler) Point Source (Probable Bos bler) Linear Contact Linear Li	M73
Games Game	41.547289 41.547275 41.549167 41.5531904 41.549563 41.549633 41.549633 41.549633 41.549633 41.549633 41.549633 41.549633 41.549633 41.549633 41.549633 41.549633 41.549633 41.549633 41.549633 41.549633 41.549633	41 6707211 41 670747 41 670643 41 670272 41 670273 41 670254 41 670254 41 660736 41 660737 41 660737	044023.1 04405.0 044095.0 044095.0 044099.4 044103.7 044113.8 044123.1 044125.1 044125.0	4590042.3 4590105.3 4590105.3 4599090.2 4599090.2 4599090.3 4599090.3 4599090.3 4599090.3 459000.3 459	2109417.1 2109313.2 2109409.2 2109409.2 2109409.2 2109673.8 2109674.8 2109674.8 210976.8 210976.8 210976.8 210976.8 210976.8 210976.8 210976.8 210976.3	603 722.7 604 3281 9 605 333.7 605 111.5 601 112.5 605 112.5	113 121 121 121 121 120 115 115 117 121 126 120 121 123 108 108 109 105 115 110 120 121 121 121 121 121 121 121 121	205.6 22.3 22.5 22.5 22.5 22.5 22.7 22.9 24.5 25.9 24.6 25.7 25.7 25.7 25.7 25.7 25.7 25.7 25.7	2.6 2.5 1.1 1.9 12.7 2.5 2.7 2.13 2.6 5.D 10.4 4.5 3.1 10.4 4.5 3.1 10.7 10.8 10.7 10.8 10.7 10.8 10.7 10.8 10.8 10.8 10.8 10.8 10.8 10.8 10.8	1.9 0.9 0.6 0.5 0.5 0.7 0.8 0.7 0.3 1.2 0.3 1.2 0.5 0.6 0.5 0.6 0.7 0.8 0.9 0.7 1.2 0.9 0.9 1.2 0.9 1.2 0.9 1.2 0.9 1.2 0.9 1.2 0.9 1.2 0.9 1.2 0.9 1.2 0.9 1.2 0.9 1.2 0.9 1.2 0.9 0.9 1.2 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9	0.7 0.6 0.2 0.3 0.3 0.3 0.3 0.1 0.1 0.2 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	Point Source Linear Centact Point Source (Probable Bos Iden) Point Source (Probable Bos Iden) Point Source (Probable Bos Iden) For Source (Probable Bos Iden) Linear Centact Linear Centac	M73
G18 G18 G19 G19 G11 G11 G11 G11 G11 G11 G11 G11	41.5421899 41.5479275 41.5491047 41.5531004 41.5495047	41 6707211 41 6707047 41 6706419 51 6701475 41 6700519 41 6700519 41 680730 41 68	040023.1 04005.0 044005.0 044005.0 044005.0 044005.0 044005.0 044103.5 044123.1 044123.1 044123.1 044123.0 044125.1 044125.1 044125.1 044125.0 044155.0	4596042.3 4596042.3 4596057.9 4599690.2 4599690.2 4599690.3 4599690.3 4596690.4 4596777.0 4596697.3 4596697.3 459678.3 4	2109417.1 2109313.2 2109409.2 2109409.2 2109414.0 2109674.8 2109674.8 2109709.6	603 722.7 604 3281 9 606 333.7 606 131.5 607 131.5	113 121 121 121 121 121 120 115 117 121 126 120 121 121 105 106 105 115 110 107 111 111 111 111 111 111 111 111	205.6 22.3 22.5 22.5 22.5 22.5 22.5 22.7 22.7 22.9 24.5 26.7 26.7 26.7 26.7 26.7 26.7 26.7 26.7	2.6 2.5 1.1 1.9 12.7 2.5 2.7 2.13 2.6 5.D 0.7 10.04 4.5 3.1 10.07	1.9 0.9 0.6 0.5 0.4 0.7 14.2 0.3 1.2 0.4 0.7 0.3 1.8 0.6 0.5 0.8 0.9 0.8 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9	0.7 0.6 0.2 0.3 0.7 0.3 0.1 0.1 0.2 0.8 0.3 0.1 0.1 0.2 0.3 0.3 0.1 0.1 0.2 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	Point Source (Linear Contact) Dear Contact Point Source (Probable Bos Iden) Point Source (Probable Bos Iden) Point Source (Probable Bos Iden) Linear Contact Linear L	M73
Gas	41.5491896 41.549197 41.5591904 41.549197 41.5591904 41.549593 41.559593 41.559593 41.559593 41.559593 41.559593 41.559593 41.559593 41.559593	41 6707211 41 670747 41 670643 41 670272 41 670273 41 670254 41 670254 41 660742 41 660747 41 660747	040023.1 04005.0 044001.9 044005.0 044005.0 044005.0 044005.0 044103.7 044113.8 044122.1 044123.0 044124.0 044125.1 044125.0	4590042.3 4590165.3 4590165.3 4590165.3 4599169.0 4599169.3 4599169.3 4599169.3 4599177.6 4599177.6 4599177.6 4599177.6 4599177.6 4599177.6 459917.3 459917.	2109417.1 2109313.2 2109409.2 2109409.2 2109409.2 2109409.2 21096714.8 21096714.8 21096714.8 2109706.8 2109706.8 2109706.8 2109706.8 2109706.3 2109707.3 2109707.3 2109707.3 2109707.3 2109707.3 2109707.3 2109707.3 2109707.3 2109707.3 2109707.3 2109707.3 2109707.3 2109707.3 2109707.3 2109707.3 2109707.3	603 722.7 604 3281 9 605 333.7 605 111.5 601 112.5 605 121.5 605 121.5 605 121.6 605 121.7 605 121.7	113 121 121 121 121 120 115 115 117 121 126 120 121 121 123 108 108 108 108 118 110 120 118 110 120 119 120 119 120 119 120 111 110 120 1119 120 1119 120 1119 120 1119 120 1119 120 1119 120 1119 120 1119 120 1119 120 1119 120 1119 120 1119 120 1119 120 1119 120 1119 120 1119 120 1119 120 1119 120 120 120 120 120 120 120 120 120 120	205.6 22.3 22.5 22.5 22.5 22.5 22.7 22.9 24.5 25.7 24.7 24.7 24.7 24.7 24.7 25.7 25.7 25.7 25.7 25.7 25.7 25.7 25	2.6 2.5 1.1 1.9 12.7 2.13 2.5 2.7 2.13 2.5 3.0 0.7 1.03 3.0 0.7 1.03 2.8 2.9 1.9 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	1.9 0.9 0.6 0.5 0.4 0.7 14.2 0.3 1.2 0.3 1.2 0.5 0.6 0.5 0.6 0.7 0.3 14.3 1.7 0.5 0.8 0.9 0.7 1.1 0.9 0.9 1.1 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9	0.7 0.6 0.2 0.3 0.3 0.3 0.1 0.2 0.3 0.3 0.1 0.2 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	Point Source Linear Centact Point Source (Probable Bos Iden) Point Source (Probable Bos Iden) Point Source (Probable Bos Iden) For Source (Probable Bos Iden) Linear Centact Linear Centac	M73

						Side	ican Sonar Con	tacts					
100	NADES G	eographic	MADES U	ITM Zone 17		tate Plane North	Bathymetry	Distance from	Length	Wide	Height	The second second	Associated Mag
10	Latitude	Longitude	East (m)	North (m)	East (US servey feet)	North (US servey feet)	(m)	Proposed Route (ne)	(m)	(m)	(m)	Description	Anomaly ID
C344	41,5433712	-81.6675183	444340.8	4599294.2	2196440.6	684828.2	11.5	80.3	2.2	13	0.6	Point Source (Probable Boulder)	2007
C345	41.5428351	-81.6672239	444348.2	4599234.7	2196168.3	681633.1	114	110.0	2.0	1.5	0.6	Point Source (Probable Boulder)	
		-81.6670194	444962.0	4596015.5	2196537.4	683258.4	11.1	280.8	6.9	0.8	-	Linear Contact	
C348		-81 6660459 -81 6667617	7.00	4596904.1	2196581.5	683615.6 685360.7	11.5	234.2 54.7	1.4	0.6	0.6	Orcular Contact Point Source (Probable	-
		-81.6666675	1,000	4596523.7	2196642.9	682302.3	10.0	540.6	4.5	0.5	0.1	Boulderj Linear Contact	+
C350		-81.6664678 -81.6664224	444405.9	4596664.8 4556430.0	2196693.1 2196712.9	682765.6 601996.1	10.3	282.2 349.3	3.9	0.6 I.6	0.1	Linear Contact Circular Contact:	
C353	41.5357122	-81.6664035	444410.5	4556443.3	2196717.7	682039.9	10.1	348.1	3.1	2.4	0.4	Rectangular Contact	100
	41.5355430	-81,6663366 -81,6661312	444411.8	4598424.5 4598415.1	2196722.9	681978.3 681948.5	10.1	343.8 930.5	6.9	0.4	0.5	Groviar Contact: Linear Contact:	M34
100	17 YOUR TO SEE	-81.6660122	444443,4	4598473.2	2196823.9	682139.8	10.0	308.6	2.0	2.0	0.4	Rectangular Contact Point Source (Probable	
C356	41.5404358			4596967.5	2196812.6	683762.1	11.3	153.5	1.7	1.0	0.5	Boulder)	
C357	41.5869531	-01.6659764 -01.6659330	444452.9	4599457.9 4598854.3	2196800.8 2196833.4	605371.6 603390.8	11.5	100.4	3.2	0.4	0.1	Linear Contact Linear Contact	+
C350	41.5393006	-81.8659024 -81.8658774	444455.5	4598923.9	2196842.1	683377.9 681978.7	11.1	181.2	3.0	0.4	0.1	Linear Contact Linear Contact	-
C362	41.5593153	-81.6657848	444465.2	4588843.0	2196874.5	683354.4	11.0	174.1	2.6	0.5	0.1	Linear Contact	
C363	41.5594764	-81.6655826	444482.2	4598860.7	2156525.3	689413.6	11.0	152.6	9.1	0.5		Linear Contact Point Source (Probable	M164
C364	41.5405681			4500501.8	2196977.6	683811.9	11.5	100.9	1.7	0.9	0.6	Boulders	ANIE
C366	41.5383879	-81.6653399 -81.6653200	444595.7	4596739.7 4599064.9	2196994.1 2196994.8	689017.6 684084.8	10.4	171.9 70.2	6.1	0.4		Linear Contact Linear Contact	M166
C167	41.5366690	-41.6652979	444503.6	4598548.7	2197917.0	602391.1	10.0	223.0	10.7	2.0		Point Source (Probable Soulder)	
CHER	41.5412280	-41.6682677	444510.0	4599052.0	2197000.5	601045.3	11.4	69.7	6.0	0.1	0.1	Linear Contact	
C350 C370	41.5436985	-01.6651522 -01.6651502	444510.0 444521.7	4596989.5 4599929.2	2197015.7 2197052.1	603037.9 604953.2	11.5	87.5 85.5	11.5	2.4	0.2	Linear Contact Circular Contact	
C371	41.5429487	-81.6649808 -61.6648749	444535.6 444535.6	4599245.8 4598544.9	2157061.9	684690.3 602390.4	11.3	46.5 191.3	2.8	2.2	-	Linear Contact Rectargular Contact	
C373	41.5404384	-81.6646158	444563.7	4596966.9	2197190.6	683766.6	11.1	43.5	6.7	0.5	0.1	Linear Contact	
C374	41.5441247	-81.6643217 -81.6641478	444593.9	4599976.0	2197256.2 2197299.4	685110.5 683562.8	10.9	169.3 33.0	5.5	0.5	0.1	Linear Contact Linear Contact	
(376	41.5402326	-81.6642375	444595.1	4598543.8	2197294.9	689692.7	11-0	20.8	5.8	0.4	-	Linear Contact	
C377	41.5429576	-81,6642185	444599.0	4599957.3	2197297.1	605049.9	11.5	164.9	10.4	3.2		Low Reflectivity Patch (Possisie Stag)	
C378		-81 6642159		4596696.6	2197300.3	683537.9	10.9	32.0	9.5	0.6		Linear Contact Point Source (Probable	
C379	41.5415479		444617.6	4599067.5	2197961.9	684099.7	11.5	37.6	1.2	1.0	0.6	Boulder)	2.43
CSEC		-01.6639251	444622.7	4599132.4	2197975.0	604312.9	11.3	61.5	5.8	0.7	0.1	Linear Contact Point Source (Probable	
CSES	41.5416010	-81.6637215 -81.6635943	444699.3	4599085.4 4598598.1	2197480 3	684192.6 683967.2	11.1	46.7	2.9	2.7	0.6	Boulder) Linear Contact	0.00
(313	41,5367471	-81.6685790	444647.5	4598556.4	2197489.0	682424.4	9.8	84.0	4.9	2.5	-	Rectangular Contact	
CHI	41.5376005			4599043.8	2197523.8 2197515.8	682735.7 684024.7	10.1	44.5 75.1	3.1	0.5	0.1	Rectangular Contact Linear Contact	M29
	41.5402331	-81.6633750	444967.0	4590543.3	2197531.0	683695.1	10.9	48.8	10.9	0.4	0.2	Linear Contact	5 (P)
30000	41.5426937	-81.6631325		4599056.4 4599236.3	2197589.3 2197583.3	684065.6 684592.2	11.2	95.8 151.9	19.3	0.6	0.1	Linear Contact Linear Contact	
C389	41.5409948	-01.6631201	444083	4599027.7	2197595.9	603973.3	11.2	95.4	1.3	0.7	0.6	Point Source (Probable Soulder)	(4)
C350	41.5572015	-81.6629816	444697.2	4596606.5	2197649.3	682591.5	10.0	21.8	1.7	1.0	1.4	Point Source (Probable Soulder)	((*))
C351		-81.6629308	444704.9	4599057.3	2157649.0	684071.2	11.1	118.0	16.5	0.5	0.2	Linear Contact	
C352	41.5412085	-81.6627034 -81.6627034	444704.9	4599053.0 4599053.0	2197645.3 2197711.4	684051.7 684058.3	11.1	116.3 134.9	5.1	0.7	0.0	Linear Contact Linear Contact	
	41.5401107		444732.0	4598929.2	2197744.9	683652.5	10.5	106.2	5.0	0.4		Linear Contact	S Tell 7
		-81.6625764 -81.6625411		4598991.7 4599038.0	2197749.9 2197756.3	683660.8 684009.8	10.6	108.5	6.0	0.6	-	Linear Contact	
		-81.6624951 -41.6621079	444740,5 444766.0	4598950,0	2197771.6 2197944.0	689721.1 684387.0	10.6	120.5 204.4	7.0	0.5		Linear Contact Linear Contact	140
COSS		-81.6621531		4596875.6	2197879.4	6020223	10.1	66.7	2.5	3.7	1.1	Point Source (Probable	-
				3.0003.0000	100000000000000000000000000000000000000		100000	100000		,,,,,,,	-	Soulder) Point Source (Probable	357.0
	100000000000000000000000000000000000000	-81.6621031		4586875.A	2197887.6 2197877.2	681822.0	10.2	69.1	1.8	1.2	0.6	Boulder)	8.5
	-	-81.6620963 -81.6620264		4599062.7 4598686.8	2197908.2	682859.8	10.2	78.6	2.0	1.5	12	Linear Contact Point Source (Probable	
-	100.00000	2012/12/12/19	Thorac Colors	2000000000		75) 545-4-X	2 2000	-	2000	-	Boulder) Point Source (Proleable	3
1000	41.5418485	-81.6620173 -81.6619165	120000000	4599121.8 4599022.2	2197897.0	684287.2	10.8	210.3	1.2	0.7	0.5	(Soy kler)	
		-81.661E759		4599043.6	2197936.2	694024.1	10.9	197.4	9.2	0.1	0.1	Linear Contact Linear Contact	
CADE	41.5419096	-01.6610404	444795.0	4599139.5	2197943.0	604310.0	11.1	225.8	1.5	0.0	3.0	Point Source (Probable Soulder)	220
CAD7	41.5409961	41.6616853	444908.6	4599026.9	2197990.7	683977.5	10.8	200.2	5.6	0.5	0.1	Linear Contact	(40)
C406		-51.6616176	1,000,000	4598855,7	2150015.8	662890.7	10.1	315.9	1.9	0.5	0.8	Point Source (Probable Soulder)	
C4106	41.5412277	-81.6614278	7000000	4599052.5	2190060.5	684062.6	10.8	256.4	5.7	0.4	0.1	Linear Contact Point Source (Probable)	
C410	41.5383226	-81.6611910	444839.2	4598729.9	2196108.2	683004.5	10.3	150.2	2.7	LE	0.7	Boulder)	8.5%
G111	41.5389529	-81 6611642	444949.0	4596733.1	2190142.0	683015.6	10.1	161.3	1.5	1.0	0.5	Point Source (Probable Boulder)	650
G112	41.5303756	-81.6611077	444854.6	4596735.6	2190150.2	683024.3	10.2	166.6	3.1	1.2	0.9	Point Source (Probable Soulder)	198-1
6813	41.5384757	-81.6610147	444552.4	4396746.7	2190183.3	683061.0	10.3	177.3	12	0.7	0.4	Point Source (Probable	100
-									-	0.550	-	Soulder) Paint Source (Probable	1 255
CASA		-81.5606008		4596758,7	2190296.2	683102.4	10.5	215.9	3.1	1.0	1.0	Soulderi	1.5
6418	41.5588604	-81.6605/811	444898.7	4598756.9	2196901.3	683129.4	10.5	218.0	2.2	1.3	0.7	Point Source (Probable Soulder)	1357
6416	41.5387020	-81,6605765	444899.1	4598771.5	2198902.4	683144.6	10.5	219.7	2.5	1.2	0.7	Point Source (Probable Boulder)	100
6417	41.5386709	-81.6605402	444902.1	4598768.1	2196912.5	683133.4	10.6	221.6	2.5	0.7	0.7	Point Source (Probable	1
G118		-81.6604032	444914.0	4596818.5	2190348.4	683299.5	10.5	247.7	3.4	LE	0.6	Boulder) Rectangular Contact	M106
C419		-01.6604102	444913.1	4596779.8	2190347.7	603172.6	10.5	235.5	2.6	1.1	0.7	Point Source (Probable Soulder)	
-												and the same of	

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_	MADES 6	eographic	MANGE O	ITM Zone 17	WATER ONLY	tate Plane North	can Soner Con	SHIRL SHOW COME					
10	Latitude	Longitude	East (m)	North (m)	East(US servey feet)	North (US servey foot)	Eathyraetry (m)	Proposed Route (nr)	Length (m)	Width (m)	Height (m)	Description	Associated May Anomaly ID
Ç420	41,5385383	-81.6603481	444918,1	4598753.2	2190965.5	683085.5	10.5	232.4	1.7	0.7	0.5	Point Source (Probable Soulder)	12 000
6421	41.5387309	-81.6602/029	444923.2	4596774.6	2100303.1	603155.9	10.7	243.6	4.0	2.2	0.7	Point Source (Probable Boulder)	1
C422	41.5586186	-81.6602/872	444923.4	4590794.3	2150381.2	603187.9	10.5	246.6	1.9	2.2	0.0	Point Source (Probable Boulder)	1
C423	41,5599666	-61.6601601	444934.9	4596911.7	2196412.0	603006.5	10.4	255.1	6.0	0.7	0.2	Linear Contact	
0434	41.5386927	-81.6601584	444934.0	4598770.2	2158416.9	683142.3	10.6	252.7	2.3	1.1	0.8	Point Source (Probable Soulder)	
6425	41.5389034	-81.6601138	OTTO STATE OF	4598793.6	2159428.4	683219.2	10.5	263.3	1.9	1.0	0.7	Point Source (Probable Boulder)	
(425	43.5407736	-81.6600747	444942.8	4599001.2	2198432.5	683900.T	10.5	328.9	2.1	1.7	0.6	Circular Contact	M26
5427	41.5189287	-81.6600659	444941.9	45907964	2100441.4	689779.5	10.5	267.9	1.6	1.0	0.9	Point Source (Probable Boulder)	-
0128	41.5396366	41.6599435	444952.7	4598874.9	2198472.4	663495.8	10.5	301.3	2.2	2.0	0.6	Rectangular Contact	+ 1
C429	41.5589773	-81.6599406	444952.4	4596801.7	2196475.5	683346.6	10.6	279.5	2.9	1.1	0.4	Point Source (Probable Soulder)	-
0430	41.5390225	-81.6599005	4449,55.0	4596808.6	2190408.3	683269.3	10.5	284.8	3.0	1.2	0.7	Linear Contact :	
6431	41.5591901	-81.6595928	444981.6	4598825.1	2198570.0	688325.0	10.4	314.3	2.2	2.3	0.7	Point Source (Probable Soulder)	M62
0432	41,5395059	-81.6594679	444992.3	4598860.1	2198603.1	683440.4	10.6	334.8	2.1	1.6	-	Rectangular Contact	M36
6434	41.5412468	-81.65918F3	445017.7	4599053.1	2198675.4	684075.3	0.0	415.7	2.2	1.6	1.5	Point Source (Probable Soutsier)	945
C435	41.5393496	-41.6591395	485019.6	4596042.4	2196693.5	603304.0	10.6	155.6	2.2	1.0	1.3	Point Source (Probable Boulder)	
5436	41.5594000	-61.6590536	445026.0	4590049,0	2190716/0	603406.1	10.6	364.5	2.5	1.4	0.7	Point Source (Probable Boulder)	-
C457	41.3394521	-81.6590459	445027.5	4500053.8	2156718/8	665421.9	10.6	366.5	2.7	1.0	0.9	Point Source (Probable Boulder)	
C438	41,5597920	41.6590282	445029.2	4590091.0	2156722.5	663543.8	10.7	579,3	5.2	2.3	0.5	Rectangular Contact	
6439	41.5394321	-81.6590259	445029.1	4586851.6	2198734.3	689414.7	10.6	367.5	2.2	0.9	0.6	Point Source (Probable Boulder)	
5440	41.5394747	-81 4589939	449031.8	4996856.3	2100733.0	683430.3	10.6	371.4	2.7	1.2	1.2	Point Source (Prolliable Boulder)	
(441	41.5398344	-81.6590029	445031.3	4596892.9	2190729.3	683550.4		383.2	2.0	2.4		Rectangular Contact	2000
0442	41.5395029	-81.6589084	445039.0	4596968.3	2190756-0	603470.0	10.7	101,0	1.3	0.5	1.0	Point Source (Probable Boulder)	4
C443	41.5594001	41.6587317	445053.6	4598848.5	2156805.0	603405.0	10.7	350.0	1.5	1.4	0.7	Point Source (Probable Soulder)	
C444	41.5398521	41.6586279	445052.7	4596896.0	2190831.6	683568.R	1-4	413.2	1.5	1.6	0.6	Rectangular Contact	
6445	41.5595078	-81.6586050	445064.3	4598859.7	2190859.3	663443,4	- 34	403.5	2.8	0.8	0.6	Point Source (Probable Boulder)	9.0
0446	41,5996563	-81.6585-672	445067.5	4596876.2	2198849.1	689497.6	1.4	411.4	14	1.0	0.5	Point Source (Probable Boulder)	
6447	41.5390272	41.6584060	445035.1	4596295.1	2100092.7	643560.3	3.3	430.0	1.6	0.0	1.0	Point Source (Probable Boulder)	3.8
5441	41,5397896	-01.6585/021	4450B.1	4590090.6	2106890.3	603546.3	3.4	430.6	2.5	1.0	0.6	Point Source (Probable Soulder)	
0445	41,5599923	41.6581954	445090.5	4596513.3	2150922.4	669629.7	141	444.3	2.5	2.5	0.7	Point Source (Probable Boulder)	100
C450	41.5398630	41.6581472	445094,4	4596898.9	2150936.0	683573.8	(ce	443.8	2.4	2.2	0.6	Point Source (Probable Soulder)	
(45)	41.5899502	-81 6581051	445098.0	4598508.6	2198947,2	688605.6	39	450.1	1.9	0.7	0.9	Point Source (Probable Boulder)	1 3 500
5452	41.5400100	-81,6581.874	445099.5	4598915.2	2199951.9	689627.5		459.5	2.1	1.0	1.0	Point Source (Prohable Boulder)	5.47
0450	41.5402440	-01.6577455	445135.6	4598540.9	2199072.0	683713.9	3	496.5	2.1	1.7	0.0	Point Source (Probable Boulder)	197
0454	41,5402700	-01.6575067	445156.5	4596543.7	2199137.3	683724.0	(4)	516.3	1.7	0.0	0.6	Point Source (Probable Soulder)	3.0
C155	41.5402653	41.6572468	445178.2	4596543.0	2199206.4	683723.0		536.8	1.7	1.4	-	Growlar Cortact	1 -

5.2 Magnetometer Results

A review of 271 line km of magnetometer data showed no historic structures (such as shipwrecks) present within the turbine and export cable survey areas.

A total of 178 magnetic anomalies were identified and mapped from the magnetometer data acquired over the Icebreaker Wind survey area. The anomaly location, type, magnitude and observations from the sidescan sonar in the area of each anomaly are listed in Table 3. Profiles of the magnetic anomalies within a 150 m (495 feet) corridor centered on the proposed route. Profiles of those outside the corridor can be found in Appendix A.

Table 3 Magnetic Anomalies Contact List

						rtometer Anomalie	8				
ID	NAD83 G	eographic	NAD83 UT	M Zone 17		North (US survey	Bathymetry	Distance	Polarity	Amplitude	Associated Sidescan
100	Latitude	Longitude	Easting (m)	Northing (m)	feet)	feet)	(m)	Proposed	No.	(nT)	Contact ID
MI	41.5960349	-81.7914838	434038.0	4605228.5	2162296.1	703716.7	16.9	93.1	Manapole	66.9	
M2	41.5727049	-81.7348227	438738.1	4602596.6	2177868.5	695347.0	15.4	92.1	Dipole	63.9	
M3	41.5707487	-81.7299932 -81.7245598	439138.9 439589.8	4602376.0	2179196.2	694645.8 693839.5	15.3	88.6 89.4	Monopole Monopole	78.5	
MS	41.5649288	-81.7160083	440299.5	4601720.1	2183041.8	692559.4	24.3	93.6	Dipole	37.0	
M6	41.5629714	-81.7112339	440695.8	4601499.5	2184354.8	691857.9	14.5	92.4	Dipole	23.3	
M7	41.5621961	-81.7094409	440844.6	4601412.2	2184648.0	691579.9	14.4	95.8	Dipole	76.8	
M8	41.5568402	-81.6963557	441930.9	4600808.7	2188446.8	689661.1	13.2	91.4	Manapole	68.6	_
M10	41.5567475 41.5540823	-81.6961940 -81.6897585	441944.3 442478.6	4600798.3 4600498.1	2188491.4 2190261.7	689627.8 688673.0	13.2	93.9 94.6	Dipole Monopole	26.7 59.6	-
M11	41.5522990	-81.6853676	442843.2	4600297.2	2191469.5	688034.4	12.5	91.7	Monopole	30,7	
M12	41.5513733	-81.6830568	445035.1	4600192.9	2192105.1	687703.0	12.4	88.9	Dipole	21.3	C252
M13	41.5510943	-81.6824088	443088.9	4600161.5	2192283.4	687603.1	12.4	90.0	Dipole	52.6	C257
M14	41.5485383	-81.6762752	443598.2	4599873.7	2193971.0	686687.5	11.9	92.2	Monopole	187.5	C285
M15	41.5397510	-81.6714626	443992.0	4598895.0 4599350.4	2195318.7	683498.3 684987.6	11.1	598.8 398.0	Monopole	10.8	-
M18 M19	41.5486196	-81.6725876 -81.6762341	443901.7 443601.7	4599882.7	2193982.0	686717.3	11.6	82.6	Monopole Dipole	15.6	C285
M20	41.5404086	-81.6720712	443941.8	4598968.4	2195149.8	683736.3	11.3	594.9	Dipole	29.2	CLUS
M24	41.5369037	-81.6676089	444311.0	4598576.4	2196383.5	682470.9	10.1	399.8	Monopole	26.3	
M25	41.5315404	-B1.6747700	443709.0	4597985.6	2194441.6	680498.1	0.0	1091.5	Dipole	145.1	
M26	41.5407863	-B1.6600479	444945.0	4599002.6	2198419.8	683905.4	10.5	331.4	Dipole	108.9	C426
M27	41.5389450	-81.6635191	444653.9	4598800.4	2197496.0	683225.4	10.3	6.2	Monopole	32.5	
M28 M29	41.5348691	-81.6682138 -81.6634084	444558.8 444662.0	4598350.9 4598653.4	2196225.0 2197531.0	681728.0 682743.5	9.7	515.9 41.7	Monopole Dipole	27.6	C384
M30	41.5394153	-81.6600664	444942.3	4598850.4	2197531.0	683405.B	10.1	284.1	Monopole	21.6	5304
M32	41.5410904	-81.6590152	445031.4	4599035.7	2198721.5	684018.9	0.0	423.7	Manapale	57.5	
M33	41.5408670	-81.6593186	445005.9	4599011.1	2198639.2	683936.7	0.0	392.1	Dipole	136.6	Accessor.
M34	41.5355832	-81.6663726	444413.0	4598429.0	2196726.6	681993.0	10.1	345.6	Monopole	22.3	C352
M35	41.5362778	-81.6651042	444519.4 444997.3	4598505.3	2197071.4	682249.4	10.0	221.5	Dipole	68.7	6111
M36 M40	41.5395686 41.5394539	-81.6594086 -81.6602418	444927.7	4598857.0 4598854.8	2198619.1 2198391.4	683463.4 683419.4	10.6	341.6 271.5	Monopole Monopole	38.6 42.6	C43Z
M41	41.5604476	-81.6996252	441661.5	4601211.4	2187540.0	690967.3	13.1	128.3	Monopole	15.0	
M42	41.5631635	-81.7063681	441101.7	4601517.5	2185685.7	691940.0	14.2	121.7	Dipole	23.9	
M43	41.5660867	-81.7134617	440512.9	4601846.9	2183734.9	692987.5	14.3	121.3	Dipole	18.4	
M44	41.5676671	-81.7172859	440195.5	4602025.0	2182683.3	693554.0	14.9	121.6	Dipole	69.5	
M45	41.5682266	-81.7187086	440077.4	4602088.1	2182292.1	693754.3	14.9	118.9	Dipole	24.7	
M46 M47	41.5690275 41.5713855	-81.7205561 -81.7263001	439924.1 439447.4	4602178.3 4602444.1	2181784.0 2180204.6	694041.6 694886.8	14.9 15.3	122.7	Monopole Monopole	133.3	_
M48	41.5713835	-81.8026381	433115.4	4605990.2	2159225.4	706163.8	17.2	121.6	Monopole	10.1	-
M49	41.6008315	-81.8006887	433275.8	4605768.1	2159764.4	705444.1	17.1	1.9	Monopole	61.0	C8
M50	41.6007495	-81.8008125	433265.4	4605759.1	2159730.8	705413.9	17.1	15.6	Manapale	49.1	CB
M51	41.6001685	-81.7991386	433404.3	4605693.3	2160190.3	705205.9	17.1	2.7	Manapale	17.0	
M52	41.5984615	-81.7950101	433746.6	4605500.6	2161324.5	704593.0	17.0	1.8	Monopole	30.2	
M53	41.5733222	-81.7339397	438812.3	4602664.5	2178108.1	695574.0	15.5	3.5	Monopole	98.0	-
M54 M55	41.5710419	-81.7284984 -81.7274535	439263.8 439350.5	4602407.5 4602357.1	2179604.2 2179691.6	694756.3 694595.8	15.3 15.2	1.7	Manapale Dipole	16.4 28.8	_
M56	41.5679312	-81.7210021	439885.9	4602056.9	2181665.5	693641.1	14.7	1.9	Dipole	16.6	
M57	41.5661370	-81.7166729	440245.2	4601854.7	2182856.0	692998.0	14.8	2.7	Dipole	155.1	
M58	41.5658378	-81.7159728	440303.3	4601821.0	2183048.6	692890.7	14.6	3.7	Dipole	84.8	
M59	41.5656580	-81.7154803	440344.2	4601800.7	2183183.9	692826.4	14.4	3.4	Monopole	134.0	-
M60	41.5576602	-81.6960083	441960.6	4600899.5	2188539.1	689960.8	13.3	2.4	Monopole	9.6	-
M63 M62	41.5512867 41.5391598	-81.6806541 -81.6595351	443235.4 444986.4	4600181.7 4598821.7	2192763.0 2198585.9	687677.7 683314.1	12.6	0.8 317.9	Monopole Monopole	9.7	C431
M65	41.5410308	-81.6583996	445082.7	4599028,7	2198890.2	683998.8	0.0	470.7	Monopole	125.3	0431
M66	41.5409427	-81.6585305	445071.7	4599019.0	2198854.7	683966.4	0.0	457.4	Monopole	233.1	
M67	41.5335442	-81.6689649	444195.0	4598204.3	2196024.0	681243.3	9.6	606,2	Monopole	25.0	
M69	41.5479070	-81.6751860	443688.5	4599802.9	2194271.3	686460.3	12.1	109.8	Manapale	29.1	
M70	41.5407007	-81.6714029	443997.8	4599000.4	2195331.7	683844.5 682810.7	11.3	530.9	Dipole Monopole	60.0	- 6315
M71 M74	41.5378505 41.5531703	-81.6696039 -81.6813766	444145.4 443176.8	4598682.8 4600391.3	2195834.1 2192558.8	688362.1	12.4	526.B 153.4	Dipole	23.2	C318
M75	41.5551699	-81.6862229	442774.4	4600616.5	2191225.6	689078.3	12.7	153.2	Monopole	29.0	C226
M76	41.5629892	-81.7051321	441204.6	4601497.3	2186024.5	691879.6	14.1	154.4	Monopole	16.4	-
M77	41.5634985	-81.7063778	441101.2	4601554.7	2185681.9	692062.1	14.2	153.9	Monopole	47.1	
M78	41.5649951	-81.7102511	440779.6	4601723.5	2184617.0	692597.7	14.5	344.0	Monopole	15.9	-
M79	41.5671708	-81.7152571	440364.2	4601968.5	2183240.0	693378.1	14.7	154.7	Monopole	13.3	
M80 M81	41.5675736	-81.7162534 -81.7210491	440281.5 439883.5	4602013.9 4602238.9	2182966.1 2181647.3	693522.4 694238.2	14.8	153.9	Monopole	27.9	
MB2	41.5717140	-81.7251910 -81.7251910	439865.5	4602480.5	2180233.4	694236.2 695006.8	15.3	157.9	Monopole monopole	19.3	C83
MB3	41.5797575	-81.7457494	437833.9	4603387.4	2174856.6	697890.6	16.0	155.9	Monopole	13.3	
M84	41.6044681	-81.8025638	433123.3	4606173.3	2159241.0	706765.0	17.2	116.9	Monopole	123.9	C6
M86	41.6028804	-81.8045865	432953.1	4605998.6	2158692.4	706182.1	17.2	123.9	Monopole	130.4	100000
M87	41.6081027	-81,8084546	432636.2	4606581.4	2157619.4	708076.5	17.A	31.5	Monopole	20.7	
M89	41.6010727	-81,8019985 -81,8019673	433166.9	4605795.9	2159405.5 2159610.1	705529.1 704950.4	17.1	72.8	Dipole	50.2	
M90 M91	41.5723577	-81.8012672 -81.7353154	433226.2 438696.7	4605618.5 4602558.4	2177734.8	704950.4 695219.3	17.1	149.6 145.6	Monopole Monopole	26.3 142.0	
M92	41.5694135	-81.7283386	439275.6	4602226.6	2179653.2	694163.3	15.2	152.1	Dipole	79.6	C63
M93	41.5681926	-81.7252617	439531.0	4602088.9	2180499.1	693725.9	15.0	147.4	Dipole	17.1	100
M94	41.5677188	-81.7242741	439612.9	4602035.6	2180770.9	693555.7	15.1	153.9	Dipole	16.7	11
M95	41.5658153	-81.7197241	439990.5	4601821.1	2182022.1	692873.3	14.6	156.5	Dipole	33.5	
M96	41.5654690	-81.7187908	440068.0	4601782.0	2182278.6	692749.4	14.8	152.7	Dipole	18.6	
M97	41.5649433	-81.7177223	440156.6	4601722.9	2182572.7	692560.4	14.7	161.0	Monopole	44.1	
M98	41.5646518	-81.7170716	440210.6	4601691.2	2182751.7	692459.5	14.5	162.3	Dipole	20.2	
M99 M100	41.5598377	-81.7160350 -81.7048125	440296.8 441228.4	4601662.7	2183036.2 2186122.4	692370.9 690732.1	14.3	145.0	Monopole Monopole	79,4	
M101	41.5589784	-81.7028964	441387.4	4601050.5	2186649.6	690423.8	13.4	146.0	Monopole	48.4	
			442984.1	4600154.8	2191919.9	687575.1	12.4	147.1	Dipole	71.5	C243

	NADEZ C	eographic	NADERLIS	M Zone 17		ntometer Anomalie tate Plane North	Element of the second	Distance			Associated
ID	100 (S10) (S10)	The state of the s	125010000	CONTRACTORS		North (US survey	Bathymetry	from	Polarity	Amplitude	Sidescan
	Latitude	Longitude	Easting (m)	Northing (m)	feet)	feet)	(m)	Proposed		(nT)	Contact ID
M103	41.5500740	-81.6813081	443179.8	4600047.5	2192588.2	687234.1	12.5	145.0	Dipole	65.3	C263
M106 M107	41.5391328	-81.6603260 -81.6850092	444920.4 442874.6	4598819.2 4600487.5	2198369.5 2191561.7	683302.2 688660.6	10.5	254.0 89.7	Monopole Dipole	17.8	C418
M108	41.5676584	-81.7179539	440139.8	4602024.5	2182500.5	693549.1	14.9	93.9	Dipole	75.2	3
M109	41.5691766	-81.7217620	439823.7	4602195.7	2181453.5	694093.0	15.0	88.8	monopole	85.5	
M111	41.5700593	-81.7239224	439644.4	4602295.2	2180859.5	694409.4	14.9	88.0	Dipole	20.9	2
M112	41.5708789	-81.7259358	439477.3	4602387.6	2180306.0	694703.1	15.2	86.9	Dipole	20.4	C87
M113	41.5710823	-81,7263759	439440.8	4602410.5	2180184.9	694776.1	15.3	89.0	Dipole	25.6	C82
M115	41.5739316	-81.7332821 -81.7344668	438867.7 438769.4	4602731.7 4602787.2	2178286.1 2177960.4	695797.6 695974.2	15.6 15.6	89.2 89.5	Manapale	23.9	
M116 M117	41.5744240	-81.7656452	436182.7	4604228.9	2169390.5	700558.3	15.7	83.0	Dipole Monopole	11.8	
M118	41.5960000	-81.7867306	434434.1	4605221.0	2163596.3	703714.5	16.9	93.9	Monopole	21.9	
M120	41.6024963	-81.8010345	433248.7	4605953.2	2159665.0	706049.9	17.1	86.5	Monopole	20.2	
M121	41.6053231	-81.8038296	433018.7	4606269.2	2158892.3	707073.8	17.3	89.9	Manapale	22.5	
M122	41.5736267	-81.7333638	438860.6	4602697.9	2178264.7	695686.3	15.5	56.2	Manapale	74.9	
M123	41.5669524	-81,7170705	440212.8 440458.0	4601945.5 4601809.2	2182744.5 2183556.9	693294.1 692860.7	14.9	60.7 61.6	Dipole	26.2 38.1	
M124 M127	41.5657431	-81.7141164 -81.6669817	444362.9	4598521.6	2196556.9	682294.1	10.0	366.3	Monopole Monopole	20.1	
M128	41.5354060	-81.6674209	444325.4	4598410.0	2196440.2	681925.7	9.8	434.9	Dipole	35.6	
M129	41.5360893	-81.6679494	444281.9	4598486.2	2196293.2	682173.3	9.9	454.1	Monopole	37.5	8
M131	41.5373226	-81.6685387	444233.8	4598623.5	2196127.5	682621.1	10.3	459.8	monopole	39.7	2
M133	41.5400208	-81.6699860	444115.4	4598924.0	2195722.0	683600.5	11.4	482.6	Monopole	21.6	-
M134	41.5408592	-81.6687921	444215.7	4599016.3	2196045.9	683909.0	11.5	347.0	Monopole	31.6	1
M135	41.5374646	-81.6670369 -01.6696015	444359.2	4598638.3 4509900.4	2196538.2	682676.8	10.2	335.5	Monopole	21.6	
M138	41.5389967	-81.6686015 -81.6694249	444230.0	4598809.4 4598987.9	2196104.5 2196823.6	683230.9 683812.8	11.0	408.8	Monopole	20.2 5.8	F121
M140	41.5508761	-81.6824508	443085.2	4600137.3	2195873.6	687523.4	11.5 12.5	112.9	Dipole Monopole	15.3	C321 C256
M141	41.5512989	-81.6836088	442989.0	4600185.0	2191954.3	687674.5	12.4	118.3	Monopole	14.3	0.230
M142	41.5524452	-81.6863740	442759.4	4600314.1	2191193.5	688085.1	12.6	117.9	Dipole	72.3	-
M143	41.5565323	-81.6963428	441931.7	4600774.5	2188451.4	689549.0	13.2	120.8	Monopole	17.2	C197
M144	41.5620845	-81.7098618	440809.4	4601400.1	2184733.2	691538.2	14.4	123.5	Monopole	10.6	C167
M147	41.5653679	-81.7178134	440149.4	4601770.1	2182546.4	692714.9	14.8	123.3	Dipole	128.2	
M148	41.5725375	-81.7352346	438703.6	4602578.3	2177756.3	695285.0	15.4	124.9	Dipole	256.8	
M149	41.5990424	-81.7993035 -81.8015504	433389.4 433203.1	4605568.4	2160148.5 2159531.2	704795.2	17.1	113.6	Manopole	19.0	_
M150 M151	41.6010881	-81.8015504 -81.8005671	433286.2	4605672.5 4605796.5	2159531.2	705126.2 705537.8	17.1	118.5 23.4	Monopole Monopole	23.5	
M153	41.6006404	-81.7995452	433370.9	4605746.0	2160077.7	705377.0	17.1	32.3	Monopole	18.5	
M154	41.5735256	-81.7336781	438834.3	4602686.9	2178179.0	695648.7	15.5	33.7	Manapale	101.9	8
M155	41.5693697	-81.7237252	439660.2	4602218.5	2180915.7	694158.6	14.9	28.8	Monopole	13.7	C102
M156	41.5686945	-81.7219413	439808.3	4602142.3	2181406.0	693916.9	14.9	34.7	Dipole	36.7	C121
M157	41.5683751	-81.7213093	439860.7	4602106.4	2181580.0	693802.1	14.8	29.0	Monopole	11.5	C129
M158	41.5675903	-81,7194811	440012.4	4602018.0	2182082.8	693520.6	14.8	26.0	Monopole	25.1	C138
M159 M161	41.5653242	-81.7165652 -81.7139834	440254.4 440468.7	4601881.0 4601762.6	2182884.7 2183594.6	693084.8 692708.4	14.8	24.7	Dipole	58.7 28.0	_
M163	41.5652091	-81.7135192	440507.3	4601749.5	2183722.0	692667.6	14.2	33.6	Dipole Dipole	91.4	-
M164	41.5396470	-81.6654948	444489.7	4598879.6	2196952.7	683476.0	11.0	139.9	Dipole	8.9	C363
M165	41.5487229	-81.6761189	443611.4	4599894.1	2194013.1	686755.2	12.3	67.9	Dipole	108.8	C287
M166	41.5382546	-81.6654769	444490.0	4598725.0	2196962.5	682968.7	20.4	185.0	Dipole	25.8	C365
M167	41.5384707	-81.6661133	444437.1	4598749.4	2196787.5	683045.8	10.6	228.4	Dipole	144,4	
M169	41.5526855	-81.6847601	442894.2	4600339.7	2191634.4	688176.8	12.5	29.7	Monopole	11.0	-
M170	41.5529418	-81.6852665	442852.2	4600368.5	2191495.0	688268.9	12.6	25.1	Dipole	26.6	-
W171	41.5569863	-81.6951401 -81.6960727	442032.4 441954.9	4600824.1 4600858.5	2188779.0 2188522.8	689717.4 689825.9	13.1	28.3 36.2	Monopole Monopole	52.0 21.4	-
M173	41.5573735	-81.6962019	441944.2	4600867.8	2188487.1	689855.8	13.3	33.3	Monopole	7.4	
W174	41.5572903	-81.6959600	441964.3	4600858.4	2188553.6	689826.1	13.2	31.7	Dipole	75.1	
M175	41.5573982	-81.6961362	441949.7	4600870.5	2188505.0	689865.0	13.2	28.3	Monopole	12.3	2
W176	41.5582030	-81.6981451	441782.9	4600961.2	2187952.5	690153.2	13.5	30.7	Monopole	17.5	
M177	41.5647373	-81.7140549	440462.2	4601697.5	2183577.0	692494.4	14.2	33.8	Dipole	58.7	- 44
W179	41.5718504	-81.7312471	439035.4	4602499.2	2178849.6	695044.2	15.2	31.7	Dipole	32.0	CSO
W181 W182	41.5758412	-81.7415576 -81.7800926	438179.6 434983.3	4602949.6 4604772.4	2176015.8 2165423.9	696473.6 702273.7	15.7	57.1 29.0	Monopole Monopole	9.3	
W184	41.6004022	-81.78UU926 -81.8011538	434983.3	4605720.8	2159638.4	705286.6	17.1	61.6	Monopole	15.8	
W185	41.5992251	-81.7985377	433453.4	4605588.1	2160357.4	704863.5	17.0	65.1	Monopole	19.6	1
W186	41.5772457	-81.7451496	437881.5	4603108.1	2175028.6	696976.8	15.6	64.5	Manapale	11.1	1/2
#187	41.5729492	-81.7345112	438764.3	4602623.5	2177952.9	695436.7	15.4	55.8	Monopole	11.6	
W188	41.5716811	-81.7313903	439023.3	4602480.5	2178810.9	694982.2	15.2	53.9	Dipole	9.7	2
W189	41.5703497	-81.7282867	439280.8	4602330.5	2179664.4	694504.6	15.2	59.0	Dipole	11.2	
W190	41.5685808	-81.7239886 01.7239886	439637.5	4602131.1	2180846.2	693870.5	15.0	58.6	Monopole	8.7	
#191 #192	41.5668192	-81.7225513 -81.7197856	439756.8 439986.3	4602065.3 4601932.6	2181241.4 2182002.0	693661.3 693238.9	14.9	57.7 61.3	Dipole Dipole	9.5 24.8	C137
/193	41.5594978	-81.7020637	441457.3	4601107.6	2186875.8	690615.1	13.3	62.1	Dipole	20.6	6237
d194	41.5594349	-81.7018892	441471.8	4601100.5	2186923.8	690592.6	13.3	61.2	Monopole	13.9	
M195	41.5579714	-81.6983177	441768.3	4600935.6	2187906.1	690068.4	13.5	60.1	Monopole	8.2	
#196	41.5571836	-81.6964709	441921.6	4600846.9	2188414.1	689786.0	13.3	62.6	Monopole	6.7	
W197	41.5566534	-81,6950753	442037.5	4600787.1	2188797.9	689596.3	13.1	58.1	Monopole	16.B	1
W198	41.5526142	-81.6852246	442855.4	4600332.1	2191507.6	688149.6	12.5	55.3	Dipole	50.7	5
W199	41.5506155	-81.6805272	443245.4	4600107.1	2192800.1	687433.4	12.5	61.0	Dipole	85.2	10000
4200	41.5487343	-81.6760171	443619.9	4599895.3	2194041.0	686759.6	11.9	62.7	Dipole	163.8	C288
W201	41.5516852	-81.6790551	443369.1	4600224.9	2193199.3	687827.0	12.4	102.2	Dipole	27.6	
VI202	41.5518646	-81.6788879 -81.7003941	443383.2 441596.9	4600244.7	2193244.5 2187331.3	687892.8 690770.0	12.4	126.4 45.2	Monopole	7.9	-
W203	41.5599115	-81.7068565	441596.9 441058.5	4601152.4 4601216.3	2185561.0	690770.0	13.1	162.2	Monopole	4.8	á
W205	41.5654662	-81.7100979	440792.8	4601775.7	2184657.4	692769.8	0.0	196.0	Dipole	61.2	-
M206	41.5649531	-81.7103442	440771.8	4601718.9	2184591.7	692582.2	14.5	136.2	Dipole	20.4	
M208	41.5663045	-81.7162442	440281.1	4601873.0	2182972.8	693060.0	14.7	30.8	Monopole	68.6	
		-81.7203077	439945.8	4602295.9	2181848.5	694428.7	0.0	235.9	Monopole	71.7	

					Marine Magne	rtometer Anomalie	5				
1	NAD83 G	eographic	NAD83 UT	TM Zone 17	NAD83 Ohio S	tate Plane North	Mark	Distance		Amplitude	Associated
ID	Latitude	Longitude	Easting (m)	Northing (m)	East (US survey feet)	North (US survey feet)	Bathymetry (m)	from Proposed	Polarity	(nT)	Sidescan Contact ID
M211	41.5683874	-81.7216561	439831.8	4602108.0	2181485.1	693805.7	14.8	16.2	Monopole	22.7	C125
M214	41.5711257	-81.7263560	439442.5	4602415.3	2180190.2	694792.0	15.3	94.1	Manapale	14.1	C82
M215	41.5713403	-81.7261749	439457.8	4602439.0	2180239.0	694870.6	15.3	122.2	Monopole	61.7	C85
M216	41.5715103	-81.7260724	439466.5	4602457.8	2180266.5	694932.8	15.3	142.9	Monopole	14.0	C86
M217	41.6001150	-81.8016471	433195.2	4605689.3	2159504.4	705180.9	17.1	113.6	Manapale	32.9	
M218	41.6028241	-81.8045222	432958.4	4605992.3	2158710.1	706161.7	17.2	123.4	Dipole	79.7	i.

Some of the magnetic anomalies were correlated to known sidescan contacts (targets). The remaining magnetic anomalies were not correlated to a sidescan contact or known lakebed installation such as a pipe or cable. There are a number of anomalies mapped on adjacent survey lines that may indicate the presence of a linear ferrous feature perpendicular to the proposed route at EKP 6.3 (Figure 18). This feature could not be identified from the sidescan or subbottom profiler data acquired over this area. An analysis of the magnetic data shows that the feature is most likely a buried steel or iron buoy block or anchor at the southwest contact with associated cable running to the northeast.

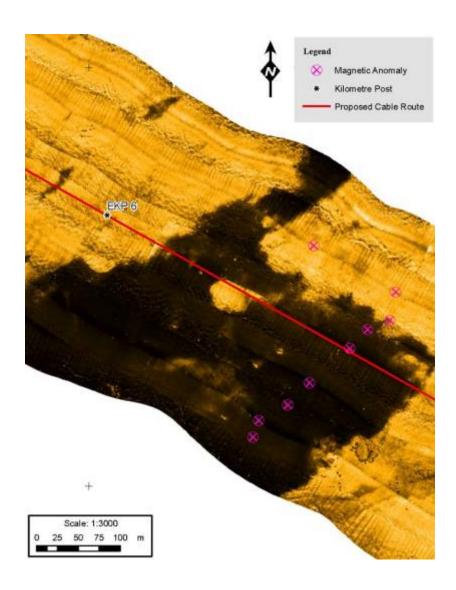


Figure 18 Location of linearly-aligned magnetic anomalies between EKP 6 and EKP 6.5. (CSR)

Past magnetic surveys in this area of the lake have also shown no correlation between the magnetic data and sidescan sonar imagery, with most of the magnetic hits having very small pole-to-pole distances indicating small or thin objects (Alpine, 2010)(VanZandt, 2015). This is primarily due to the proximity of the area being close to shore and used as a dumping ground for the past 200 years. Even today there are 5 dumping grounds identified on the latest Moss Point to Vermilion NOAA chart 14826 (Figure 19).

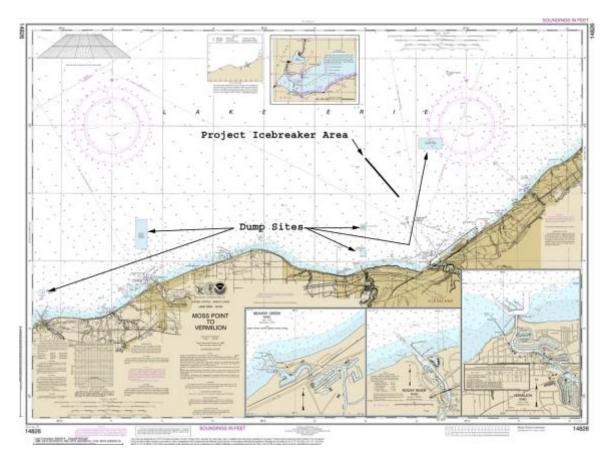


Figure 19 Current Dump Sites in Survey Areas (NOAA, VanZandt Engineering)

It is possible that some of the more magnetically intense anomalies are manmade but have no archaeological context, thus do not represent potentially significant resources. The less magnetically intense objects are most likely a function of geology, perhaps representing small pockets of glacial till or other magnetic rocks/sediment near the surface. In both cases, the Sidescan sonar imagery did not show any objects that would correlate with the anomalies. The lack of correlation is likely due to the magnetic objects being masked by overlying sediment.

5.3 Sub-bottom Data Analysis

A review of 271 line km of sub-bottom data showed no historic structures (such as shipwrecks) or artifacts were present within the turbine, export cable, and inner harbor areas.

The presence of gas charged sediments within the Icebreaker survey area was interpreted from chirp sub-bottom profiler and boomer seismic data. The presence of gas charged sediments can accentuate sub-bottom reflectors causing "bright spots" as well as prevent the penetration of the acoustic energy from the profiling system, thereby masking the acoustic signal.

The origin of the near surface gas in the survey area cannot be determined from the data collected from this survey. This gas may originate from shallow decomposed organic material (biogenic) or from deep underlying bedrock formations (petrogenic). In this area the biogenic source is plausible since vegetation has been buried during the numerous lake transgressions. This burial and subsequent decomposition could account for the presence of sub-surface gas.

Small localized erosional depressions or channels have been identified near the proposed WTG ICE1 turbine location (Figure 20) and over the near shore survey area. These features are infilled and were likely formed by glacial fluvial processes.

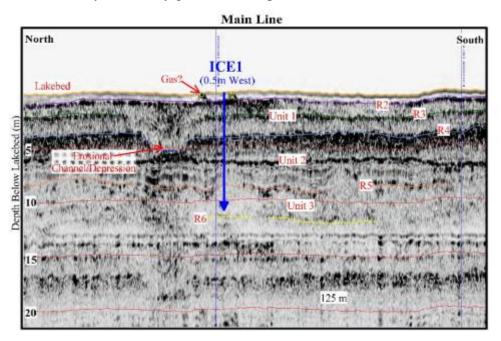


Figure 20 ICE 1 Erosional Depression or Channel (CSR)

6.0 SECTION 106 REVIEW RESULTS

The purpose of this review was to determine if any prehistoric/historically significant artifacts, such as shipwrecks or human occupation sites, might be present in the three APEs in the construction area of the Icebreaker Wind project.

6.1 Prehistoric Results

During the period from ~12,000 YBP to ~5,400 YBP the lake level was below the survey site so the possibility of prehistoric occupation sites does exist. A review of the Dames & Moore and Alpine geological data does not indicate the existence of any potential river systems or water sources that may have provided occupation sites for Paleoindians. A further literature review did not identify any past or ongoing research for the identification of prehistoric Lake Erie river systems.

Several small localized erosional depressions or channels were identified near the proposed ICE1 turbine location and over the nearshore survey area. These features are infilled and were likely formed by glacial fluvial processes. It is highly unlikely that these features contain prehistoric artifacts because erosional and sedimentation processes would have affected any prehistoric sites. This erosion would have mixed -- and destroyed -- the context of any site (Gray & Pape, 2014).

The impact of the project's construction to any prehistoric archaeological sites in the area would be negligible due to the small footprint that the foundation will occupy. Even though the mono bucket will be approximately 17.5 m (57 feet) in diameter and penetrate a maximum of 10 m (33 feet) deep into the lake bed and also into the glacial till layer, the disturbance area is small. This is due to the fact that the portion penetrating the lake bottom is only a cylindrical shell, like a biscuit cutter, not a solid object. The skirt thickness of the mono bucket is 3.175 cm (1.25 inches). The estimated surface area of disturbance for each WTG site is only 3.5 square meters (38 square feet). This coupled with the fact that the sub-bottom geology does not indicate any riverine structures leads to the conclusion that it is very unlikely that any prehistoric sites existed

in the turbine APE or that its installation would impact such a site if it were to penetrate one at a thickness of 3.175 cm (1.25 inches.)

The interconnect cables in the turbine APE are buried at a depth of 1.5 m (4.5 feet) which is above these glacial till deposits. Their installation would not impact any potential prehistoric site.

The export cable, running to shore, is buried at a depth of 1.5 m (4.5 feet) and disturbance width of 1.5 m (4.5 feet). Several possible paleo-depressions/channels have been interpreted from the sub-bottom geology data and these are below the burial depth of the export cable. Any disturbance to any possible prehistoric site due to the small disturbance area seem unlikely.

The borehole for the HDD export cable will be well below any potential prehistoric site. The 0.6 m (18 inch) borehole will run from the breakwater, through the inner harbor, and exit at the CPP substation at a total depth of 18 - 27 m (60 - 90 feet) bottom level and a minimum of 4 m (12 feet) below the foundation of the breakwater.

6.2 Historic Results

No properties of historical significance were identified by the survey at the Icebreaker Wind APEs.

7.0 CONCLUSIONS AND RECOMMENDATIONS

Results from the Section 106 review have confirmed that there were no artifacts or properties of historical significance identified within the Icebreaker Wind APEs. Moreover, the literature search produced no evidence of the existence of any artifacts or properties within the project's proposed APEs.

Based on this review, VanZandt Engineering concludes that the Icebreaker Wind project will have no impact on historic properties. VanZandt Engineering believes that no further archaeological investigation is required for this project and that project construction be approved. However, while the research and survey work for this project were thorough, no survey technique is completely adequate to identify all cultural resources in a given area. In the unlikely event any historic or prehistoric remains are discovered during project construction, the SHPO and/or VanZandt Engineering should be contacted to investigate and evaluate the significance of any such finds.

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Exhibit BB

Section 106 Geophysical Survey Review for Icebreaker Wind

Appendix A

Icebreaker Offshore Wind Demonstration Project 2016 Marine Geophysical Survey Results

CONFIDENTIAL

FILED UNDER SEAL

Icebreaker Windpower Incorporated has requested confidential treatment of Appendix A to this document in accordance with OAC Rule 4906-2-21.

Appendix A to Exhibit BB contains critical infrastructure information, confidential research and development information, or commercial information, trade secrets, and/or proprietary information and, as such, is entitled to confidential treatment under state and/or federal statutes and regulations.

An unredacted version of Appendix A has been submitted to the Docketing Division of the OPSB in accordance with OAC Rule 4906-2-21(D)(2).

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Summary: Application - Part 12 of 13 Exhibit BB electronically filed by Christine M.T. Pirik on behalf of Icebreaker Windpower Inc.