

FILE

BEFORE

THE PUBLIC UTILITIES COMMISSION OF OHIO

In the Matter of Protocols for the  
Measurement and Verification of Energy  
Efficiency and Peak Demand Reduction  
Measures.

Case No. 09-512-GE-UNC

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GAS UTILITIES JOINT COMMENTS AND OBJECTIONS REGARDING  
DRAFT TECHNICAL REFERENCE MANUAL

Pursuant to the Commission's Entry of October 4, 2010, The East Ohio Gas Company d/b/a Dominion East Ohio ("DEO"), Columbia Gas of Ohio, Inc. ("Columbia") Vectren Energy Delivery of Ohio, Inc. ("VEDO") and Duke Energy Ohio, Inc. ("DE-Ohio") (together, the "Gas Utilities") jointly file these consensus comments and objections to the draft Technical Reference Manual ("TRM") docketed on August 6, 2010.

I. COMMENTS

The Commission's October 4, 2010 Entry invited industry stakeholders to file "objections" to the draft TRM. In addition to the specific objections discussed below, the Gas Utilities have several overarching comments that the Commission should also consider.

First, it is important for the Commission to understand that the Gas Utilities do not have the personnel or resources to perform a comprehensive review of the draft TRM. Unlike the electric utilities, the Gas Utilities are not subject to the energy efficiency standards imposed by S.B. 221. Nevertheless, during recent rate cases the Commission approved voluntary energy efficiency programs for all of the Gas Utilities. Some of the energy efficiency programs approved by the Commission include many of the same features included in the draft TRM, including engineering data and measurement and verification. Each of the Gas Utilities

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participates in a stakeholder process to develop and administer these programs. As a result of rate case commitments, the Gas Utilities must necessarily devote their resources to administering programs already approved through the consensus stakeholder process. The Gas Utilities have therefore focused their review of the draft TRM on specific measures that may effect existing programs.

Second, the Commission should take into consideration the fact that the Gas Utilities are currently in the process of approving, or have recently approved, energy efficiency programs for calendar year 2011. These programs were developed through the stakeholder process. To the extent the Commission requires the Gas Utilities to observe the final version of the TRM, it should not do so until 2012 at the earliest. The Gas Utilities do not believe they should be required to follow the final TRM, for the reasons discussed in earlier comments filed in this docket.

Third, and again assuming the TRM eventually becomes mandatory for the Gas Utilities, the Commission should ensure that it is flexible and inexpensive to administer. There is a cost to gather all of the data so that sponsoring utilities can: (a) produce an application for program approval; (b) demonstrate that the program is cost effective; (c) provide appropriate measurement and verification; (d) develop new programs; (e) annually amend existing programs to meet ongoing requirements; and (f) participate in continuous regulatory proceedings to amend the TRM. Many of these activities may be necessary, but they should be designed to minimize time and cost. The TRM should be a flexible guide, not a static document with prescriptive, inflexible mandates.

The objections that follow should be taken into consideration along with the foregoing comments.

## **II. OBJECTIONS**

### **Attic Insulation (Draft TRM, p. 36)**

Columbia's consultant was unable to match the HDD60 values listed for Toledo, which may point to a similar problem with other city weather data. The consultant downloaded the weather data from the University of Dayton source cited (which is no longer at the URL listed; it has changed to <http://academic.udayton.edu/kissock/http/Weather/default.htm>) and was unable to match the TRM values. The consultant found an average of 4819 HDD60 per year for the 14 years with at least 360 days of data (it is unclear how the TRM process dealt with missing days from the cited source) yet the TRM lists 4482 HDD60, which is lower than any extended period Columbia could find. The Gas Utilities recommend that the HDD table calculations used throughout the TRM be rechecked and verified.

### **Showerheads (Draft TRM, p. 93)**

The TRM savings are based on one fairly detailed metering study done in Canada, but the savings figure may be too low depending on housing characteristics and program design. The TRM takes measured overall DHW savings of 16 therms from homes with existing showerheads using 2.0-2.5 gallons per minute (gpm) and then divides this by the average 2.1 showerheads per home, and further divides this figure by 1.2 change in gpm (2.45 gpm pre - 1.25 gpm post) to arrive at 6.6 therms per showerhead per gpm reduction as the savings. But that same study found average savings of 31 therms for homes where the existing showerhead flow rate was measured as >2.5 gpm. It appears that those saving would be a larger per showerhead per gpm reduction, although the report does not contain sufficient details, citing "personal communication with the authors" as the source of showers per home. (p. 95, fn. 245.)

The biggest issue here is that 2.1 showerheads per home seems high and would be expected to lead to lower savings per showerhead. Replacing showerheads that people actually use should result in savings greater than the 6.6 therms/yr/gpm. Columbia assumes greater savings of 13 therms/yr/showerhead based on the replacement of showerheads actually used. The draft TRM does not provide a basis for assumptions concerning the second and third showerheads per home.

Additionally, the TRM uses high flow rate assumptions (2.87 gpm existing), which are based on full flow of the showerhead. Columbia's consultant's calculations are based on considerably lower flow rates, which are representative of throttled flow. Using the TRM default flow rate of 2.87 and an assumed new flow rate of 1.6 results in savings of 8.4 therms per showerhead. Adopting the TRM would require the use of the TRM's higher flow rate, resulting in less savings.

#### **Pipe Insulation (Draft TRM, p .97)**

The draft TRM calculations appear to be acceptable, assuming that the water heater does not have heat traps to stop thermosiphoning. However, modern water heaters typically have this feature to boost their energy factor (EF) rating. There is a typo (top of p.98 at footnote 251) where the TRM references outside air temperature, where basement (or DHW pipe area) temperature was probably intended. This should be clarified.

#### **Wall Insulation (Draft TRM, p. 100)**

The TRM does not accurately describe how to calculate the R value of an insulated wall. According to the TRM, "An R-value of 5 should be assumed for the wall assembly plus the R-value of any existing insulation." (p. 100.) R-5 is a proper assumption for an un-insulated wall, but the wall does not become R-18 when R-13 insulation is added to the stud cavities. The wall

is only about R-13 overall. The TRM should provide a more detailed calculation method based on framing factor assumptions, such as the following formula:

$3 + 1/ (.25/5 + .75/\max(1.6, R_{ins}))$ , where

3 = R value of the interior and exterior sheathing and air films; this would be added to overall cavity R value estimate.

The denominator of the fraction calculates the U value of the interior of the wall cavity (or  $UA$  where Area ( $A$ )=1 sq.ft.)

.25 = 25% framing factor, 25% of the wall is framing

5 = R value at framing

.75 = 1- framing factor = fraction of wall area that is cavity

$\max(1.6, R_{ins}) = 1.6$  if there is no cavity insulation, otherwise it equals the R value of the cavity insulation.

The R value of the interior of the wall cavity is calculated as  $1/U$ . This is the second term which is added to the R-3 first term to give total wall R. This would result in R-5 for empty and R-12.4 for R-13 cavity insulation.

Alternatively, the assumed R-value after retrofit should be the rated R value of the cavity insulation. The only directly additive R value would be for insulating sheathing applied to the interior or exterior of the wall surface.

An additional problem with the existing TRM is that both examples show an upgrade to R-20 from wall insulation, which is not representative of what we can be achieved by blown cavity insulation, which is usually done when wall cavities in residential construction are 3.5" to 4" deep.

There is a typo on page 102. In the first sentence beneath the chart at the top of the page, "attic floor" which should be replaced with "wall."

There is the same HDD60 problem as mentioned under attic insulation.

#### **Air Sealing (Draft TRM, p. 104)**

The TRM cooling savings from air sealing fails to include latent gains, which would increase savings by 3 or 4 fold over the sensible-only calculations used. For heating savings, the

TRM does not explain where to derive the N factor for estimating natural air leakage. The TRM only provides a cooling N factor. Also, in the heating example, the TRM uses 4569 HDD60 for Toledo but in the table on the prior page the TRM lists 4482. There is also the same HDD60 problem as mentioned under attic insulation.

#### **Duct Sealing (Draft TRM, p.108)**

The TRM method 1 appears to make little sense. It uses modified blower door subtraction to calculate the CFM50 of duct leakage, but then treats that leakage as a natural leakage rate – implying a 50Pa pressure difference across the leak all the time. This simplified approach does not consider the location of the ducts, the supply/return split, regain factors, the operation of the system, and many other factors. It leads to low estimates for cooling savings but very high estimates for heating savings – a 171 th/yr savings (nearly 25% of heating) for a small 109 CFM50 reduction in duct leakage. There is no reference to any outside source for such a calculation procedure. The TRM also neglects latent loads associated with the air leakage for cooling.

Additionally, the TRM method 2 relies on rough estimates from a visual inspection and assumes low cooling loads when such measures might be targeted at homes with high cooling loads. The HDD60 table should be reviewed as mentioned previously regarding attic insulation.

#### **Residential new construction (new homes) (Draft TRM, p. 136)**

The User Defined Reference Home (UDRH) does not account for clothes washers. Savings from ENERGY STAR clothes washers can be captured and reported along with off-REM coincident peak and related calculations. The TRM should propose values for gas and electric hot water savings as well as direct electric savings from the washer itself.

The TRM should also confirm that the Gas Utilities should use the stated UDRH refrigerator default usage (585 kWh) as shown in the continuation of Table 3 on page 141 under "Lights and Appliances" when a refrigerator is not supplied by the builder. Otherwise, using the RESNET default will result in negative savings relative to the UDRH default.

The TRM should confirm that "0.8 DSE" listed in the continuation of Table 3 on page 141 refers to Duct System Efficiency and that the corresponding UDRH syntax is "DuctLeakageEstimate: Average".

The incremental cost assumptions in Table 4 seems high. The cited Massachusetts-based study may not be a good proxy for new home construction costs in Ohio. Research by Columbia's Residential New Construction program DSM implementer suggests that Ohio incremental costs are likely to be lower.

#### **Water Heaters (Time of Sale) (Draft TRM, pp. 123-24)**

The deemed savings for this measure should be clarified. The deemed savings for this measure is shown in the algorithm on page 123 as:  $\text{Savings } \Delta \text{MMBtu} = 180 * (1/ \text{EFBase} - 1/ \text{EFEff})$ . However in the reference section on page 124 the algorithm is shown as:  $\Delta \text{MMBtu} = \text{BtuHWUSAGE} * (1 - \text{EFBase} / \text{EFEff})$ . The TRM should clarify which algorithm is correct.

### **III. CONCLUSION**

The Gas Utilities appreciate the opportunity to present comments and objections to the draft TRM. A flexible approach to the development of gas energy efficiency portfolios is necessary to achieve accurate results and maximize benefits for customers, consistent with the process currently used by the Gas Utilities.

Respectfully submitted,

Stephen Seiple by memo per telephone approval  
Stephen B. Seiple  
Brooke E. Leslie  
Columbia Gas of Ohio, Inc.  
200 Civic Center Drive, PO Box 117  
Columbus, Ohio 43215  
Telephone: (614) 460-4648  
Facsimile: (614) 460-4944  
sseiple@nisource.com  
bleslie@nisource.com

ATTORNEYS FOR COLUMBIA GAS OF  
OHIO, INC.

Mark A. Whitt  
Mark A. Whitt  
Carpenter Lipps & Leland LLP  
280 Plaza, Suite 1300  
280 North High Street  
Columbus, Ohio 43215  
Telephone: (614) 365-4100  
Facsimile: (614) 365-9145  
whitt@carpenterlipps.com

ATTORNEY FOR THE EAST OHIO GAS  
COMPANY D/B/A DOMINION EAST OHIO  
AND VECTREN ENERGY DELIVERY OF  
OHIO, INC.

Amy B. Spiller by memo per telephone approval  
Amy B. Spiller  
Elizabeth H. Watts  
Duke Energy Ohio, Inc.  
155 East Broad Street, 21<sup>st</sup> Floor  
Columbus, Ohio 43215  
Telephone: (614) 222-1331  
Facsimile: (614) 222-1337  
Elizabeth.watts@duke-energy.com  
Amy.spiller@duke-energy.com

ATTORNEYS FOR DUKE ENERGY OHIO,  
INC.



## CERTIFICATE OF SERVICE

I hereby certify that a copy of the foregoing Gas Utilities' Joint Comments and Objections to the Draft Technical Reference Manual was sent by U.S. mail, postage paid to the following parties on this 3rd day of November, 2010.



Mark A. Whitt

Duane Luckey, Section Chief  
Office of the Ohio Attorney General  
Public Utilities Section  
180 East Broad Street, 9<sup>th</sup> Floor  
Columbus, OH 43215  
Duane.luckey@puc.state.oh.us

Sally Bloomfield, Esq.  
Bricker & Eckler LLP  
100 South Third Street  
Columbus, OH 43215-4291

Office of the Ohio Consumers' Counsel  
Jeffery Small, Esq.  
10 West Broad Street, Suite 1800  
Columbus, OH 43215-3485  
small@occ.state.oh.us  
serio@occ.state.oh.us

Carolyn S. Flahive, Esq.  
Thompson Hine LLP  
41 South High Street Suite 1700  
Columbus, OH 43215-6101  
carolyn.flahive@thompsonhine.com

Kathy J Kolich, Esq.  
FirstEnergy Corp  
76 South Main Street  
Akron, OH 44308

Mary W. Christensen, Esq.  
Christensen Christensen Donchatz  
Kettlewell & Owens  
100 East Campus View Blvd., Suite 360  
Columbus, OH 43235  
mchristensen@columbuslaw.org

Rodger A. Kershner, Esq.  
450 West Fourth Street  
Royal Oak, MI 48067-2557  
rkershner@howardandhoward.com

Steven Millard  
200 Tower City Center  
50 Public Square  
Cleveland, OH 44113

Mr. Kenneth D Schisler  
Enernoc, Inc.  
75 Federal St., Suite 300  
Boston, MA 02110  
kschisler@enernoc.com

Garrett A Stone, Attorney At Law  
Brickfield, Burchette, Rim & Stone, P.C.  
1025 Thomas Jefferson Street N.W.  
8th Floor, West Tower  
Washington, DC 20007

Randall V Griffin, Chief Regulatory  
Counsel  
Dayton Power and Light Company  
1065 Woodman Drive  
P O Box 8825  
Dayton, OH 45401

W Jonathan Airey, Esq.  
Vorys, Sater, Seymour and Pease LLP  
52 East Gay Street Po Box 1008  
Columbus, OH 43216-1008  
wjairey@vorys.com

Mr. Nolan M Moser  
The Ohio Environmental Council  
1207 Grandview Ave.  
Columbus, OH 43212-3449  
nolan@theoec.org

Gregory J Poulos, Attorney  
The Office of the Ohio Consumers'  
Counsel  
10 West Broad St., Suite 1800  
Columbus, OH 43215-3485

Ms. Christine M Falco  
PJM Interconnection LLC  
965 Jefferson Avenue  
Norristown, PA 19403  
falcoc@pjm.com

Matthew S. White, Esq.  
Chester Willcox & Saxbe  
65 E State Street  
Columbus, OH 43228  
mwhite@cwslaw.com

Mr. Dwight N. Lockwood  
Global Energy, Inc.  
312 Walnut Street, Suite 2300  
Cincinnati, OH 45202  
dnlockwood@globalenergyinc.com

Elizabeth H Watts, Esq.  
Assistant General Counsel  
Duke Energy Ohio, Inc.  
155 East Broad Street, Suite 2100  
Columbus, OH 43215  
elizabeth.watts@duke-energy.com

Ms. Connie L Lausten  
V.P. Regulatory and Legislative Affairs  
New Generation Biofuels  
4308 Brandywine St. NW  
Washington, DC 20016  
cllausten@newgenerationbiofuels.com

Mr. Steven T Nourse  
American Electric Power Service  
Corporation  
1 Riverside Plaza, 29th Floor  
Columbus, OH 43215  
stnourse@aep.com

Gary S Guzy, Esq.  
General Counsel  
APX Inc  
5201 Great America Parkway #522  
Santa Clara, CA 95054

David C Rinebolt  
Ohio Partners For Affordable Energy  
231 West Lima St  
P O Box 1793  
Findlay, OH 45839-1793

Robert J Triozzi, Esq.  
Director of Law  
Cleveland City Hall  
601-Lakeside Ave, Room 206  
Cleveland, OH 44114-1077

Ms. Kari Decker  
APX  
2939 27th St  
Sacramento, CA 95818  
kdecker@apx.com

David R. Marchese  
Haddington Ventures, L.L.C.  
2603 Augusta, Suite 900  
Houston, TX 77057

Joseph V. Maskovyak  
Ohio State Legal Services Association  
555 Buttles Avenue  
Columbus, OH 43215-1137

Dayton Power & Light Company  
Dona Seger-Lawson  
1065 Woodman Drive  
Dayton, OH 45432

Judi L Sobecki, Attorney at Law  
1065 Woodman Drive  
Dayton, OH 45432

Environment Ohio-Environmental  
Advocate  
Amy Gomberg  
203 East Broad Street, Ste 3  
Columbus, OH 43215

Greenfield Steam & Electric  
Neil Sater  
6618 Morningside Drive  
Brecksville, OH 44141

Industrial Energy Users of Ohio  
Samuel C. Randazzo  
21 E. State Street, 17th Floor  
Columbus, OH 43215

Joseph M. Clark  
McNees Wallace & Nurick LLC  
21 East State Street, 17th Fl.  
Columbus, OH 43215-4228

Ohio Energy Group, Inc.  
David Boehm  
36 E. Seventh Street, Suite 1510  
Cincinnati, OH 45202

Michael Kurtz  
Boehm, Kurtz & Lowry  
36 East Seventh Street, Suite 1510  
Cincinnati, OH 45202

Ohio Farm Bureau Federation, Inc.  
Dale Arnold  
Director Energy Services  
P.O. Box 182383  
Columbus, OH 43218

Ohio Fuel Cell Coalition  
737 Bolivar Road  
Cleveland, OH 44115

Rolls-Royce Fuel Cell Systems, Inc.  
6065 Strip Avenue NW  
North Canton, OH 44720

Sierra Club Ohio Chapter  
Brandi Whetstone  
131 N High St., Ste. 605  
Columbus, OH 43215

The Climate Registry  
Ann McCabe  
1543 W. School St  
Chicago, IL 60657

United Steel Workers District 1  
Dave Caldwell  
777 Dearborn Park Land, J  
Columbus, OH 43085

Mid Ohio Regional Planning Commission  
Erin Miller  
111 Library Street, Suite 100  
Columbus, OH 43215

Vertus Technologies Inc  
Joseph Koncelik  
2500 Key Center  
127 Public Square  
Cleveland, OH 44114-1230

FirstEnergy Solutions Corp.  
Lou D'Alessandris  
341 White Pond Drive  
Akron, OH 44320

APX Inc  
5201 Great America Parkway  
#522  
Santa Clara, CA 95054

Morgan Parke, Attorney at Law  
FirstEnergy Service Company  
76 South Main Street  
Akron, OH 44308

BrightPath Energy LLC  
33 West 19th Street  
4th Floor  
New York, NY 10011

AARP  
Ron Bridges  
17 South High Street  
Suite 800  
Columbus, OH 43215

Buckeye Power, Inc.  
P.O. Box 26036  
Columbus, OH 43226-0036

American Municipal Power-Ohio Inc  
Marc Gerken, P.E., President  
2600 Airport Drive  
Columbus, OH 43219-2266

Citizen Power  
David Hughes, Ex. Dir.  
2121 Murray Avenue  
Third Floor  
Pittsburgh, PA 15217

John Bentine  
Chester Wilcox & Saxbe, LLP  
65 East State Street, Suite 1000  
Columbus, OH 43215-4259

Theodore Robinson  
Citizen Power  
2424 Dock Road  
Madison, OH 44057

American Wind Energy Assoc.  
1101 14th Street NW  
12th Floor  
Washington, DC 20005

Citizens for Fair Utility Rates  
Tim Walters  
c/o The May Dugen Center  
4115 Bridge Avenue  
Cleveland, OH 44113

Appalachian People's Action, Coalition  
Michael R. Smalz  
Ohio State Legal Service Assoc.  
555 Buttles Avenue  
Columbus, OH 43215

Joseph Meissner  
Director of Urban Development  
Attorney at Law  
1223 West Sixth Street  
Cleveland, OH 44113

Steven L Beeler Assistant Director of Law  
City of Cleveland Department of Law  
601 Lakeside Avenue  
Room 106  
Cleveland, OH 44114

City of Hamilton  
Charles S. Young  
345 High Street  
Hamilton, OH 45011

City of Toledo  
One Government Center  
Suite 2250  
Toledo, OH 43604

Leslie Kovacik  
420 Madison Avenue, 4th Fl  
Toledo, OH 43624

Cleveland Electric Illuminating Company  
76 South Main Street  
Akron, OH 44308

Mr. Mark A Hayden  
FirstEnergy Corp  
76 South Main Street  
Akron, OH 44308

Cleveland Housing Network  
2999 Payne Avenue  
Cleveland, OH 44114

Columbus Southern Power Company  
1 Riverside Plaza  
Columbus, OH 43215

M. Howard Petricoff  
Vorys, Sater, Seymour & Pease  
52 East Gay Street  
P.O. Box 1008  
Columbus, OH 43216-1008

Council of Smaller Enterprises  
Steve Millard  
100 Public Square, Suite 201  
Cleveland, OH 44113

Direct Energy Services LLC  
Ron Cerniglia  
40 Columbine Drive  
Glenmont, NY 12077

Edgemont Neighborhood Coalition  
Ellis Jacobs  
333 West First Street, Suite 500B  
Dayton, OH 45402

Empowerment Center of Greater  
Cleveland  
3030 Euclid Avenue, Unit 100  
Cleveland, OH 44115

Global Energy  
Dwight N. Lockwood, Group Vice  
President  
312 Walnut Street, Suite 2300  
Cincinnati, OH 45202

Great Lakes Energy Development Task  
Force, Cuyahoga County, Ohio  
100 East Campus View Blvd.  
Suite 360  
Columbus, OH 43235-4679

Integrus Energy Services, Inc  
Teresa Ringenbach  
300 West Wilson Bridge Road  
Suite 350  
Worthington, OH 43085

Communities United for Action  
Noel M. Morgan, Attorney  
Legal Aid Society of Southwest Ohio  
215 E. Ninth Street Suite 200  
Cincinnati, OH 45202

Constellation NewEnergy, Inc.  
David I. Fein  
550 W. Washington Blvd, Suite 300  
Chicago, IL 60661

Interstate Gas Supply, Inc.  
Vincent Parisi  
5020 Bradenton Avenue  
Dublin, OH 43017

The Kroger Company  
Mr. Denis George  
1014 Vine Street-G07  
Cincinnati, OH 45202-1100

John Bentine  
Chester Wilcox & Saxbe, LLP  
65 East State Street, Suite 1000  
Columbus, OH 43215-4213

KW Solar Solutions LLC  
Robert Wevodau  
250 Corporate Blvd Suite D  
Newark, DE 19702

Legal Aid Society of Cleveland  
Joseph Meissner  
Urban Develop Off  
1223 W. Sixth St  
Cleveland, OH 44113

Lucas County Commissioners  
Lance Keiffer  
711 Adams, 2nd Floor  
Toledo, OH 43624

Midwest Energy Efficiency Alliance  
645 N. Michigan Avenue  
Suite 990  
Chicago, IL 60611

Natural Resources Defense Council  
2 N Riverside Plaza  
#2250  
Chicago, IL 60606-2600

Neighborhood Environmental Coalition  
Rev. Mike Frank, Co-Chair  
5920 Engle Ave.  
Cleveland, OH 44127

NOPEC  
31320 Solon Road, Ste 20  
Solon, OH 44139

Norton Energy Storage, L.L.C.  
4083 S. Cleveland-Massil  
Number 196  
Norton, OH 44203-5642

Langdon D Bell  
Bell & Royer Co., LPA  
33 South Grant Avenue  
Columbus, OH 43215

Michael K Lavanga  
Brickfield, Burchette, Ritts & Stone, P.C.  
1025 Thomas Jefferson Street N.W.  
8th Floor West Tower  
Washington, DC 20007

Barth E Royer  
Bell & Royer Co LPA  
33 South Grant Avenue  
Columbus, OH 43215-3927

Ohio Farmers Union  
20 S. Third Street  
Columbus, OH 43215

Ohio Hospital Association  
Richard L. Sites  
155 E. Broad Street, 15th Floor  
Columbus, OH 43215-3620

Ohio Partners for Affordable Energy  
Colleen L Mooney  
1431 Mulford Rd  
Columbus, OH 43212

Sierra Club Ohio Chapter  
Jennifer Miller  
131 N. High Street, Suite 605  
Columbus, OH 43215

SunEdison  
12500 Baltimore Avenue  
Beltsville, MD 20705

The Solid Waste Authority of  
Central Ohio  
4239 London Groveport Road  
Grove City, OH 43123

Dennis Hirsch  
Porter Wright Morris & Arthur  
41 S. High Street  
Columbus, OH 43215

United Clevelanders Against Poverty  
May Dugan Center  
4115 Bridge Avenue  
Cleveland, OH 44113

Thomas O'Brien  
Bricker & Eckler LLP  
100 South Third Street  
Columbus, OH 43215

Ohio Interfaith Power and Light  
Gregory E. Hitzhusen, MD  
P.O. Box 26671  
Columbus, OH 43226

Ohio Manufacturers Association  
Eric L. Burkland, President  
33 North High Street  
Columbus, OH 43215-3005

Vertus Technologies Inc  
Joseph Koncelik  
2500 Key Center  
127 Public Square  
Cleveland, OH 44114-1230

Wind on the Wires  
1619 Dayton Avenue  
Suite 203  
Saint Paul, MN 55104